

**Working with Pierre Foray to understand the  
behaviour of piles driven in sand**

**Pierre Foray Homage**

**27<sup>th</sup> January 2015**

Richard Jardine

## Background

Topic central for current large, multi € bn offshore wind-energy and hydrocarbon projects

Difficult, considered fully resistant to 'theoretical refinement' by Terzaghi & Peck

Conventional API & other approaches have poor reliability

Advances made in 25 years of Anglo-French research, last decade working with Pierre Foray and Grenoble 3S-R Lab

Continuing collaboration with France: SOLCYP, TC-209, Grenoble 3S-R and **current PISA** tests

Programme started in 1990 with Labenne field experiments with Prof Roger Frank's LCPC team

# IC instrumented piles

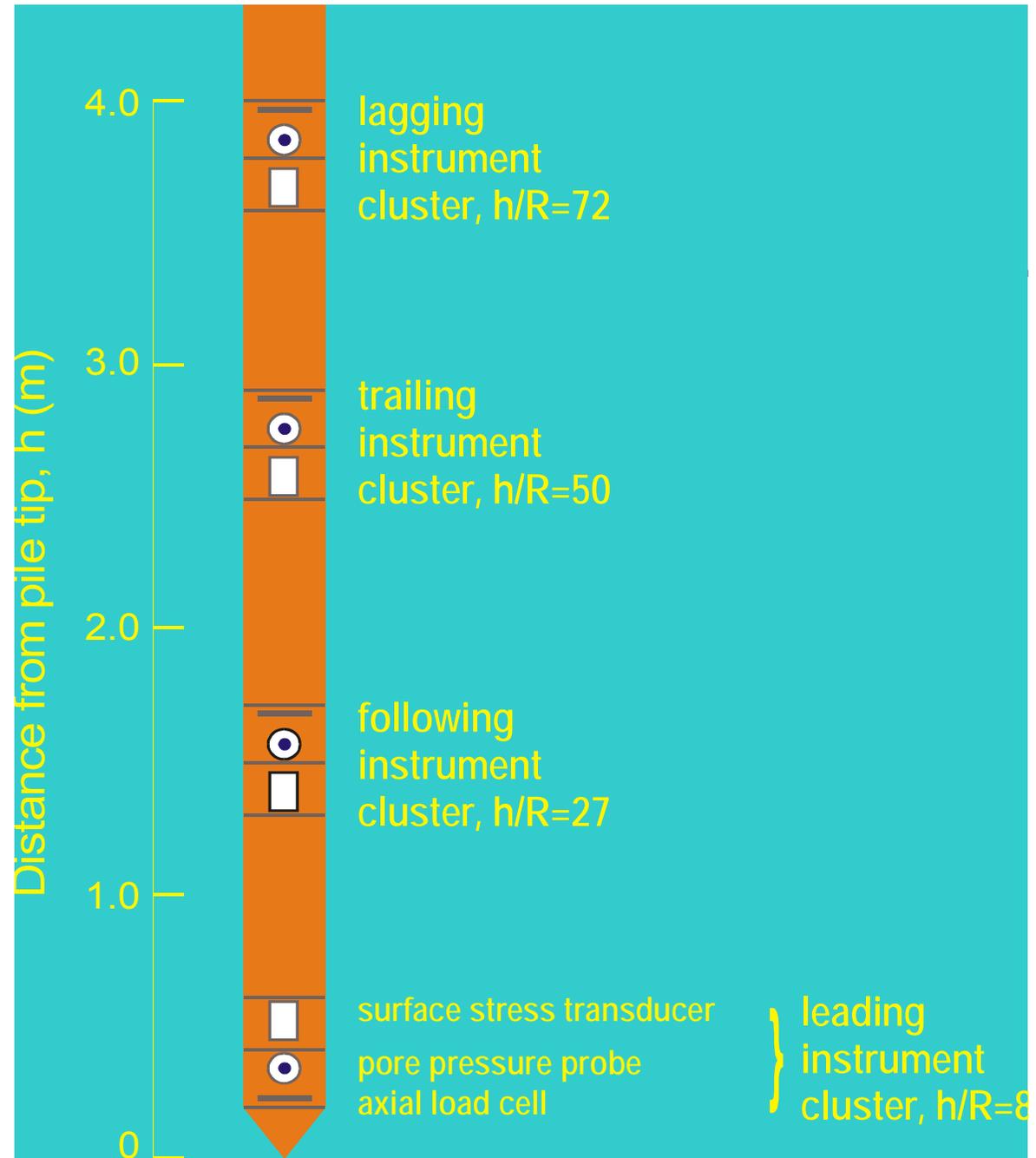
102mm diameter; up to 20m long

SSTs measure local  $\sigma_r$  and  $\tau$  on shaft

Intensive testing in sand at Labenne and Dunkerque 1990-95

...and 4 UK clay sites 1985-96

Bond, Jardine & Dalton (1991)



# The 4 + 2 Anglo-French team at Labenne, SW France, 1990

See Lehane, Jardine, Bond & Frank (1993), ASCE



## Interrogating nature...

Do conventional theories work? Constant K earth pressures and  $N_q$  models? Or direct in-situ test methods?

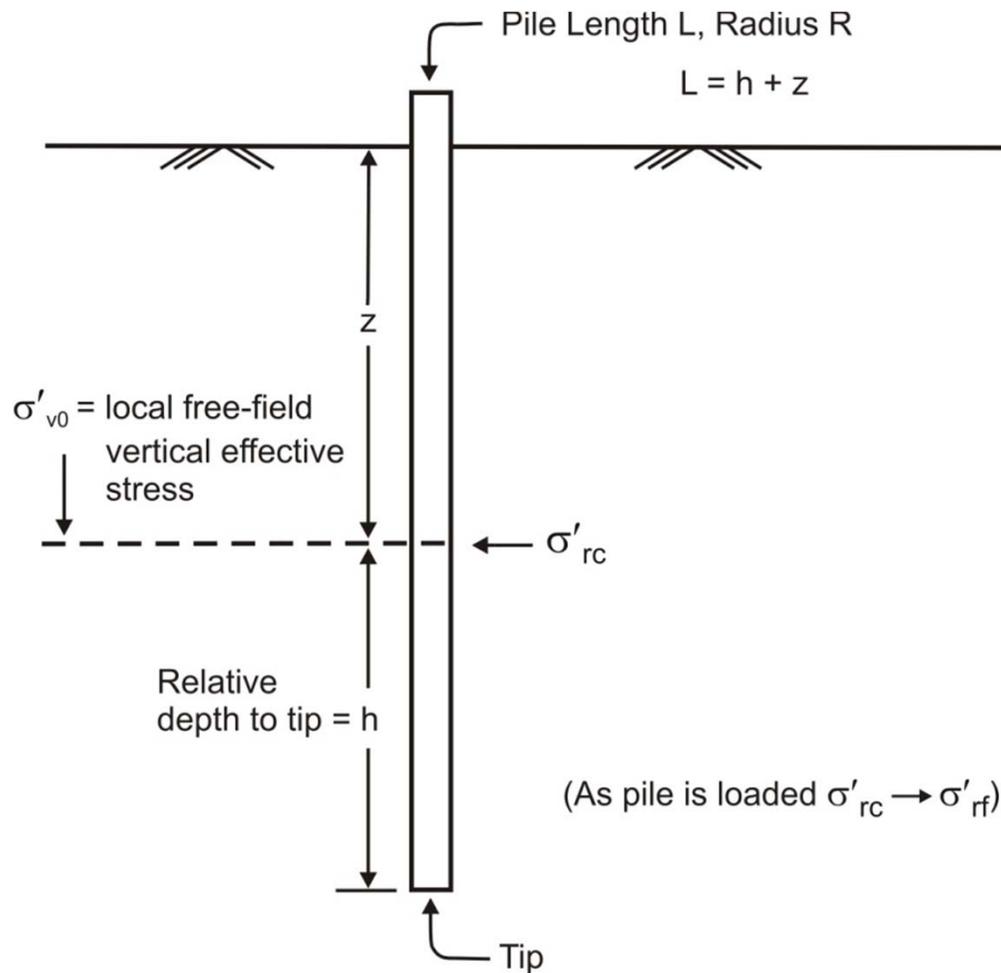
If not, what really controls failure shaft shear  $\tau$  and normal  $\sigma'_{rf}$  stresses & end-bearing  $q_b$ ?

What are the missing key variables?

Are there really upper limits to  $\tau$  and  $q_b$ ?

Compression versus tension loading?

# ICP Configuration



Multiple tests:

Loose dune sand: Labenne

Dense marine sand:

Dunkerque

Continuous profiles of shaft radial and shear stresses, axial loads and tip resistance

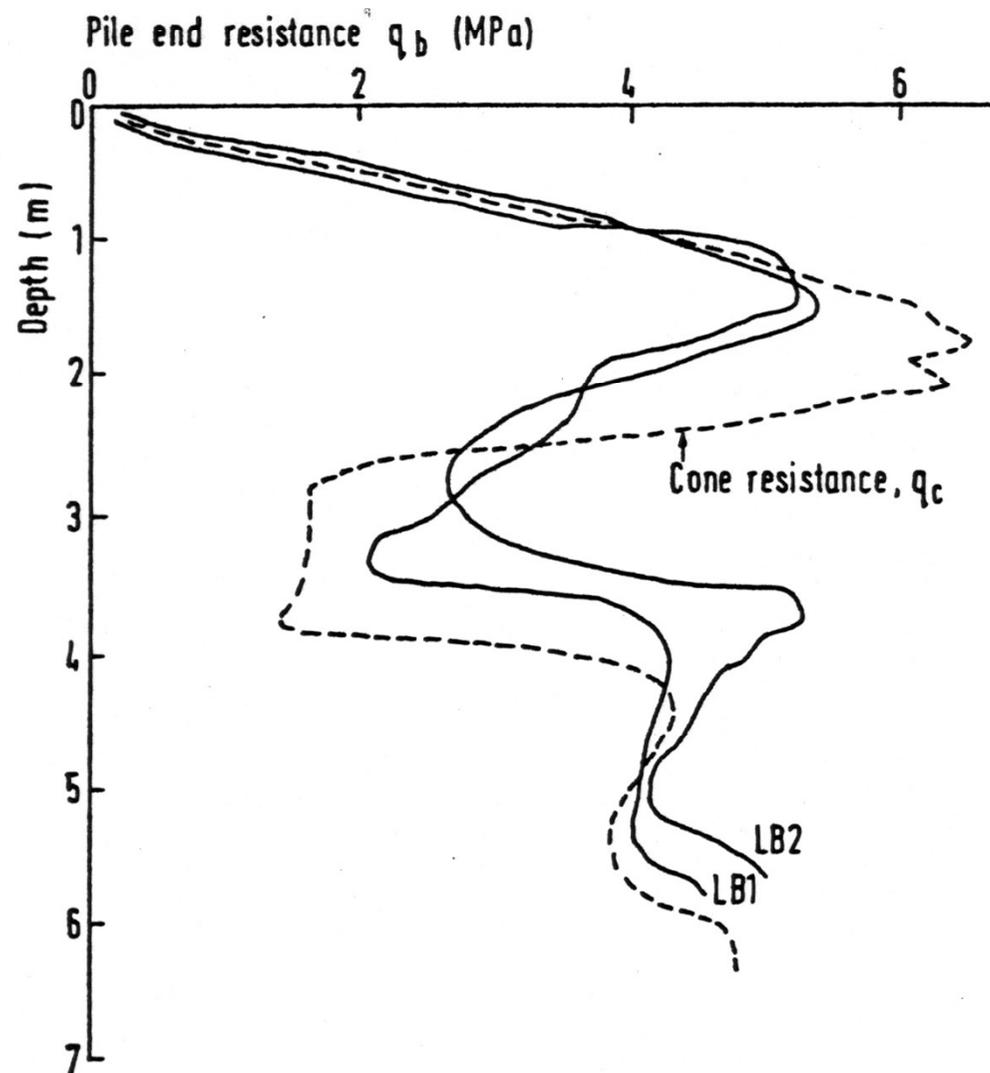
Installation, equalisation and loading to failure

Tip pressures controlled by local  $q_c$ ; shaft stresses also vary with pile tip position  $h$

Shaft stresses vary strongly during loading

# Labenne: end bearing

Pile end resistance  $q_b$  mirrors CPT  $q_c$



# Local shaft radial effective stresses

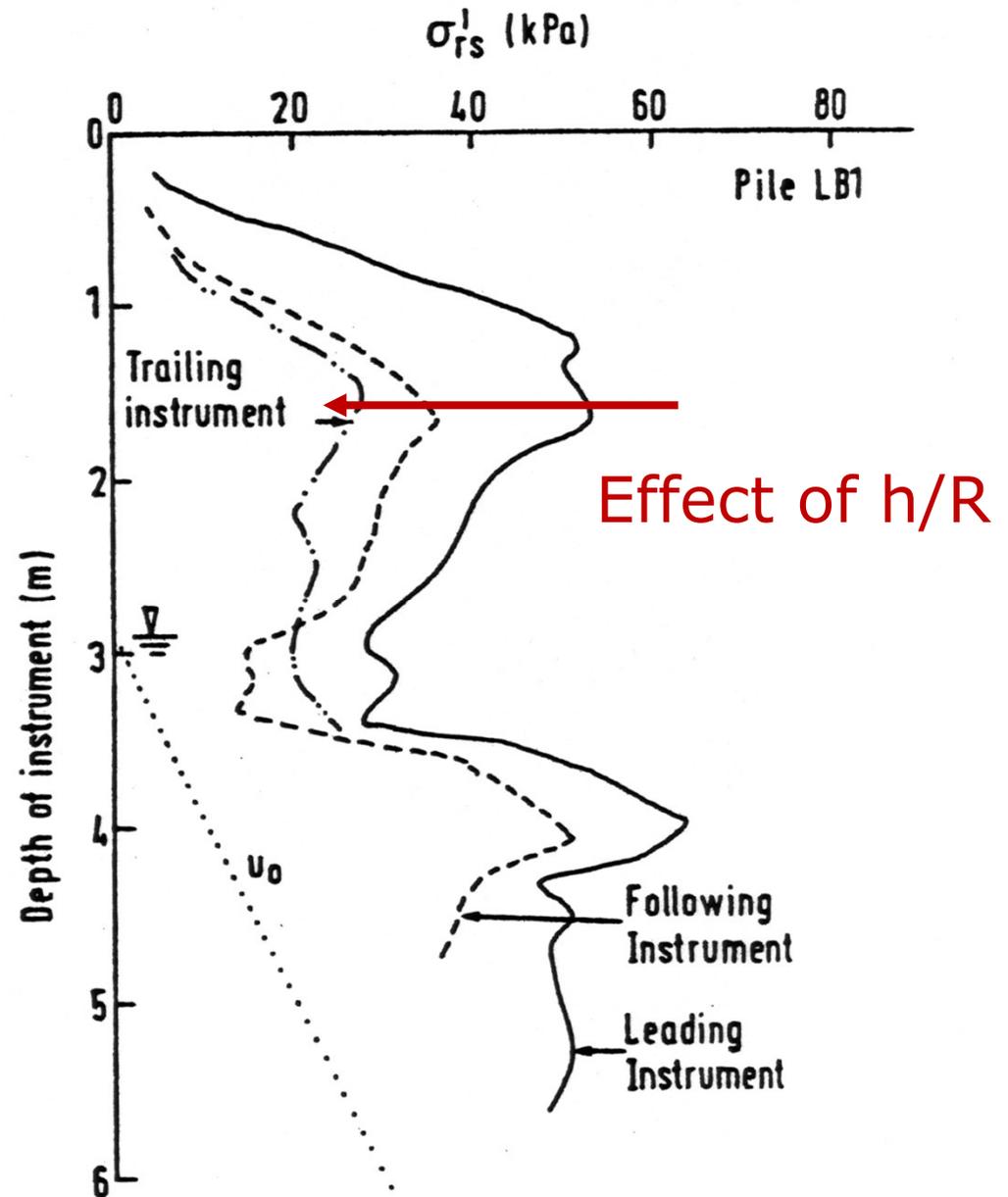
Shaft  $\sigma'_r$  during penetration at Labenne

Mirror  $q_c$  profile & vary with pile tip depth  $h$

No constant  $K$ , but

$$\sigma'_r = f(q_c, \sigma'_{vo}, h/R)$$

Confirmed in dense Dunkerque sand



# Loading response & effective stress paths, similar at Dunkerque and Labenne

$\sigma'_r$  varies under load

Tension  $\neq$  compression

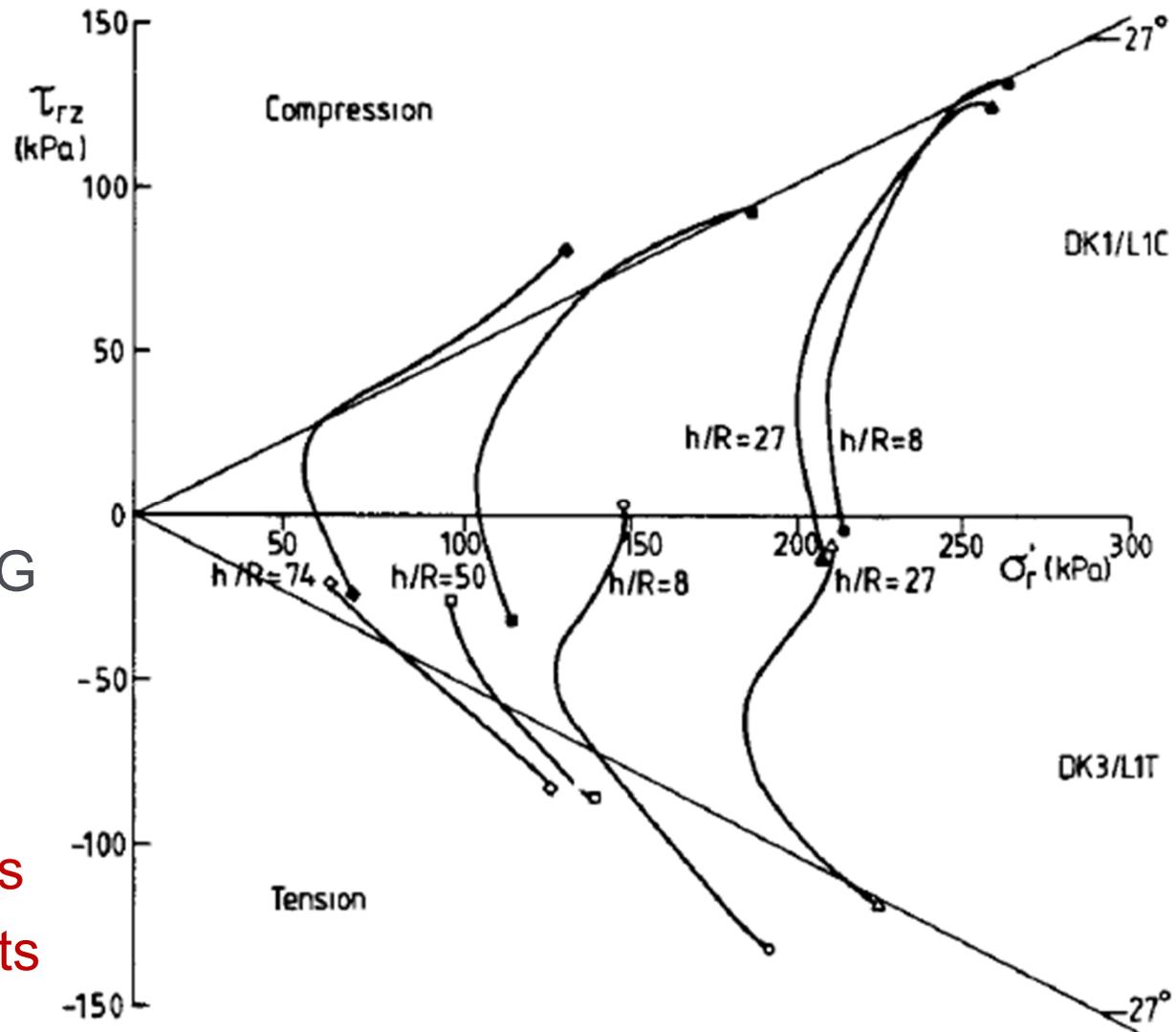
Simple interface law

$$\Delta\sigma'_{rd} = 2G \delta r/R$$

$D_r$  influence is through  $G$

$\delta_{cv}$  not affected by  $D_r$

Tests on CLAROM piles explore open-end effects



# Basis for new ICP design rules used for oil, gas & wind energy



Overy 2007



Piled tripods for Borkum West II  
German N. Sea Merritt et al 2012

Image courtesy of Trianel

## Practical impact: one large UK jacket based windfarm

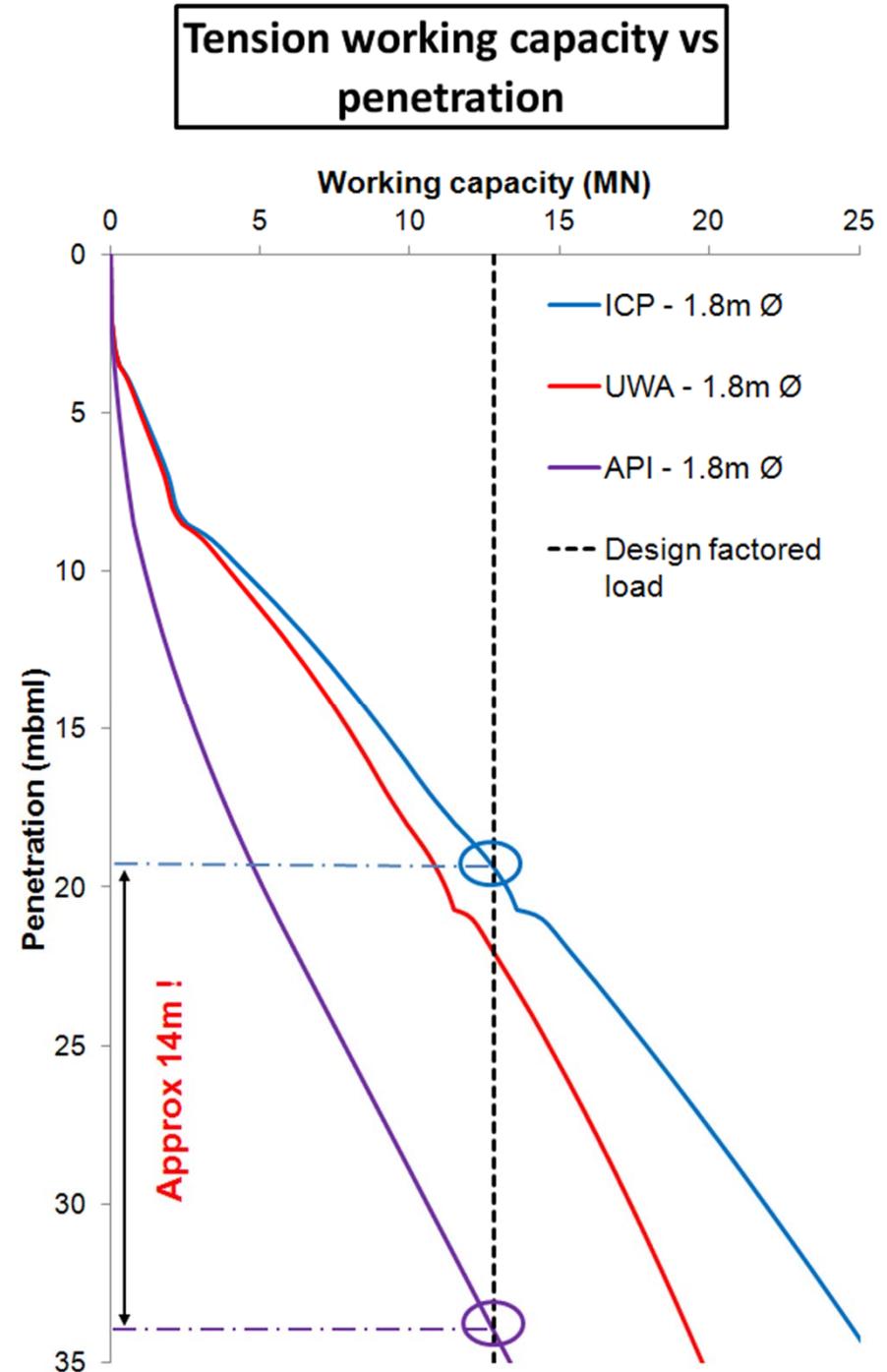
Critical economies in onshore and offshore projects

But surprising ageing results from large scale Dunkerque tests:

1994 Re-tests on CLAROM piles:  
Chow, Jardine, **Brucy & Nauroy**  
Geotechnique 1997

1998-9 tests on fresh GOPAL piles

And cyclic tests on GOPAL Piles



# Dunkerque tests in dense marine sands: 1988-2015

CLAROM, ICP, GOPAL, SOLCYP and **current PISA** tests

Variable  $q_c$  profile, up to 30 MPa

GOPAL: 8 steel pipe piles 457mm OD, 19m

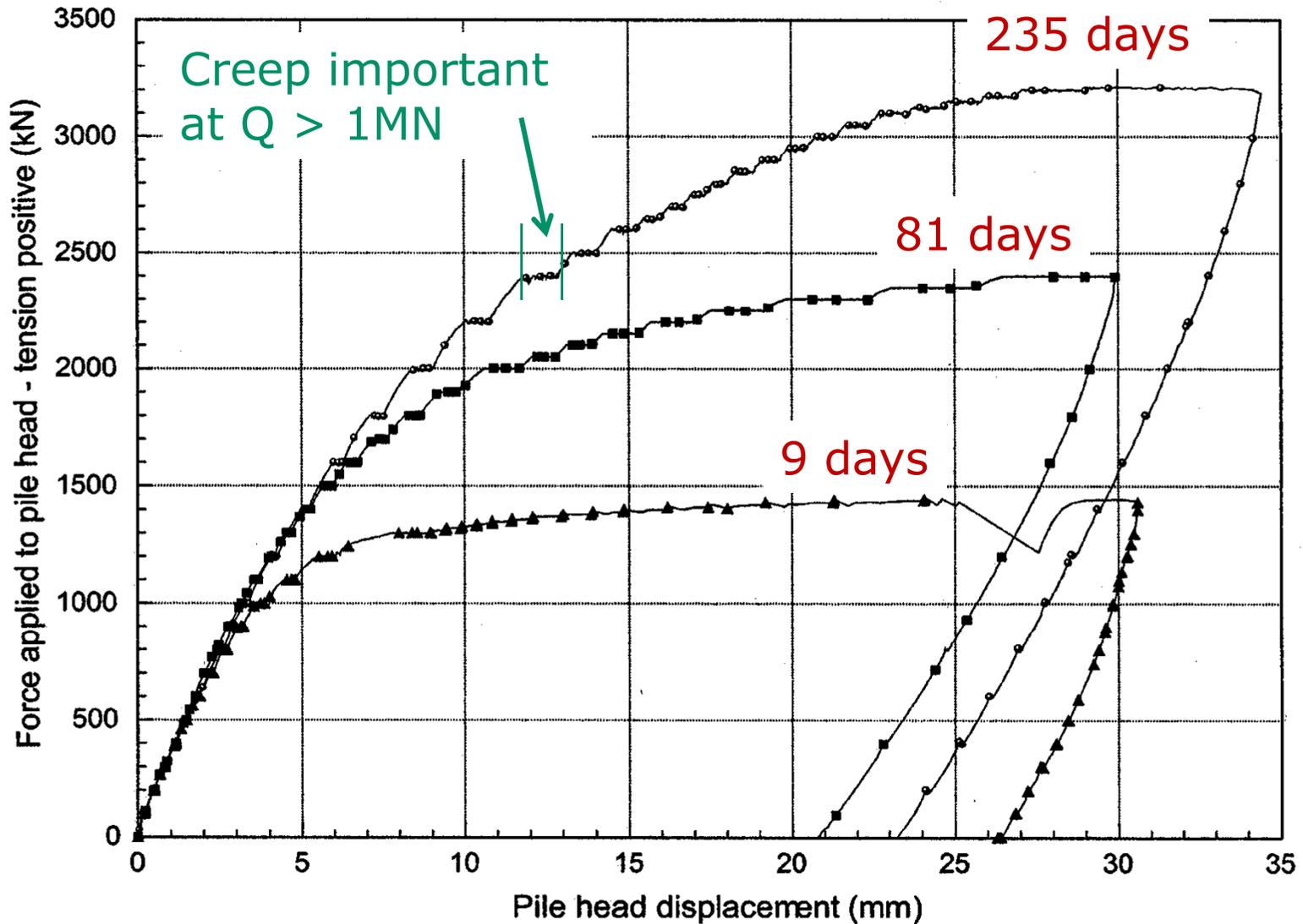
Static & cyclic loading

Pile ages: 9 days to 1 year after driving



Jardine et al 2006, Jardine & Standing 2012

# Ageing, creep & non-linear axial shaft stiffness,



1<sup>st</sup> tension tests varying with age

# Impact of axial cyclic loading

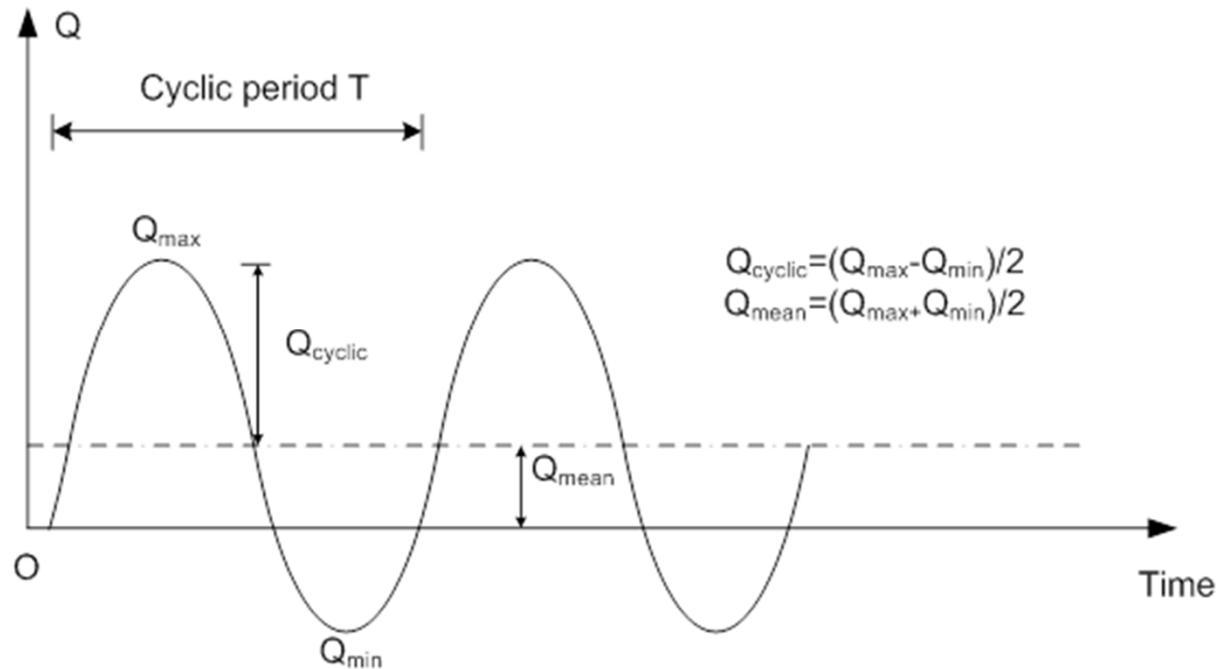
Load controlled

$T = 60s$

One-Way: tension

Two-Way: tension  
& compression

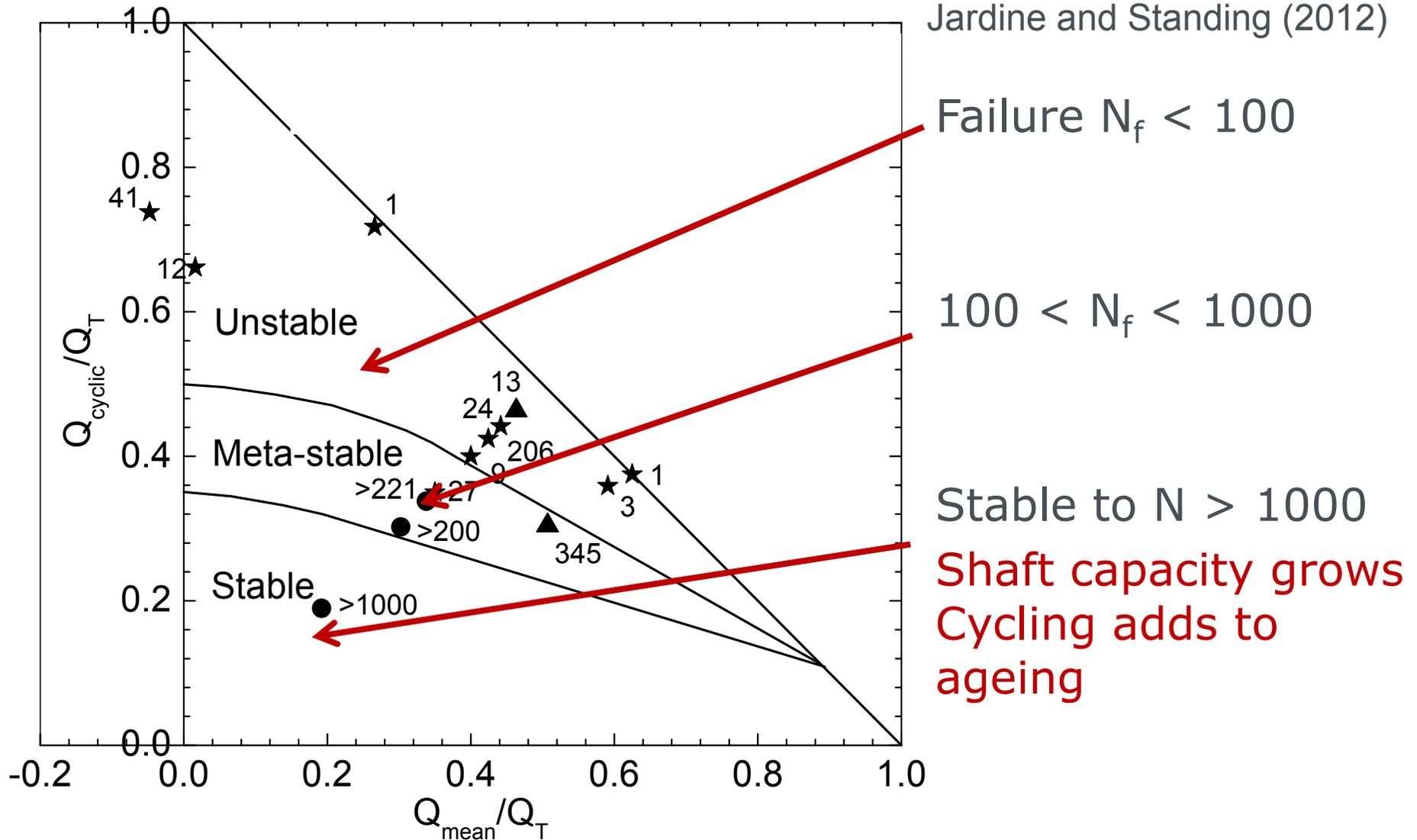
Plus: tension tests  
to failure



Failure depends on  $N$ ,  $Q_{cyclic}$ ,  $Q_{mean}$  & static tension capacity  $Q_T$

Loads normalised  $Q_{cyclic}/Q_T$  &  $Q_{mean}/Q_T$  to allow for age & pre-testing

# Impact of axial cyclic loading: can halve capacity

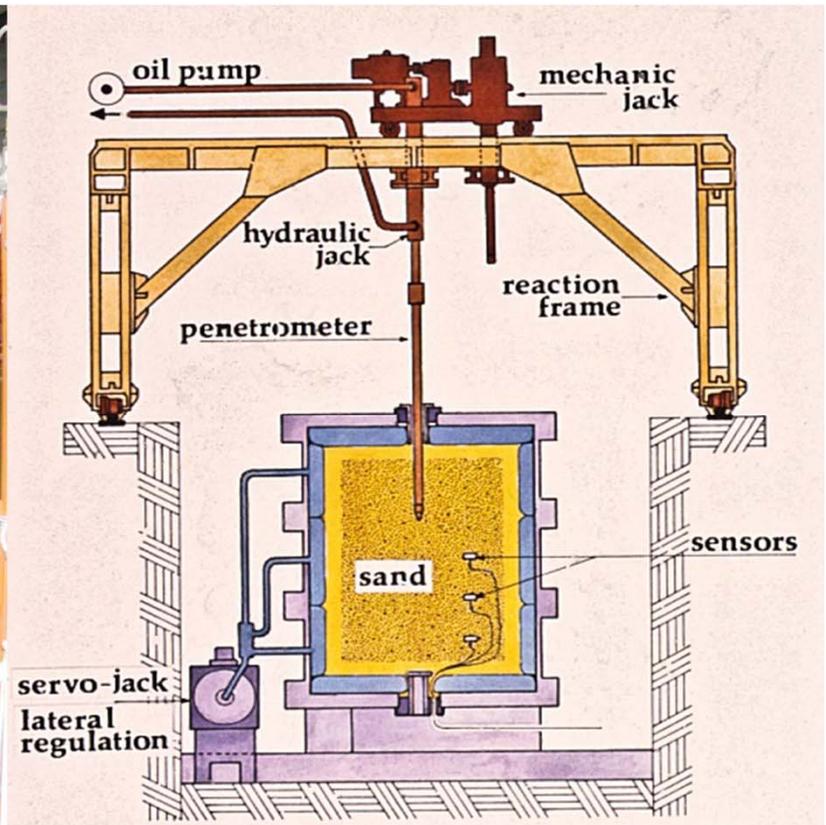
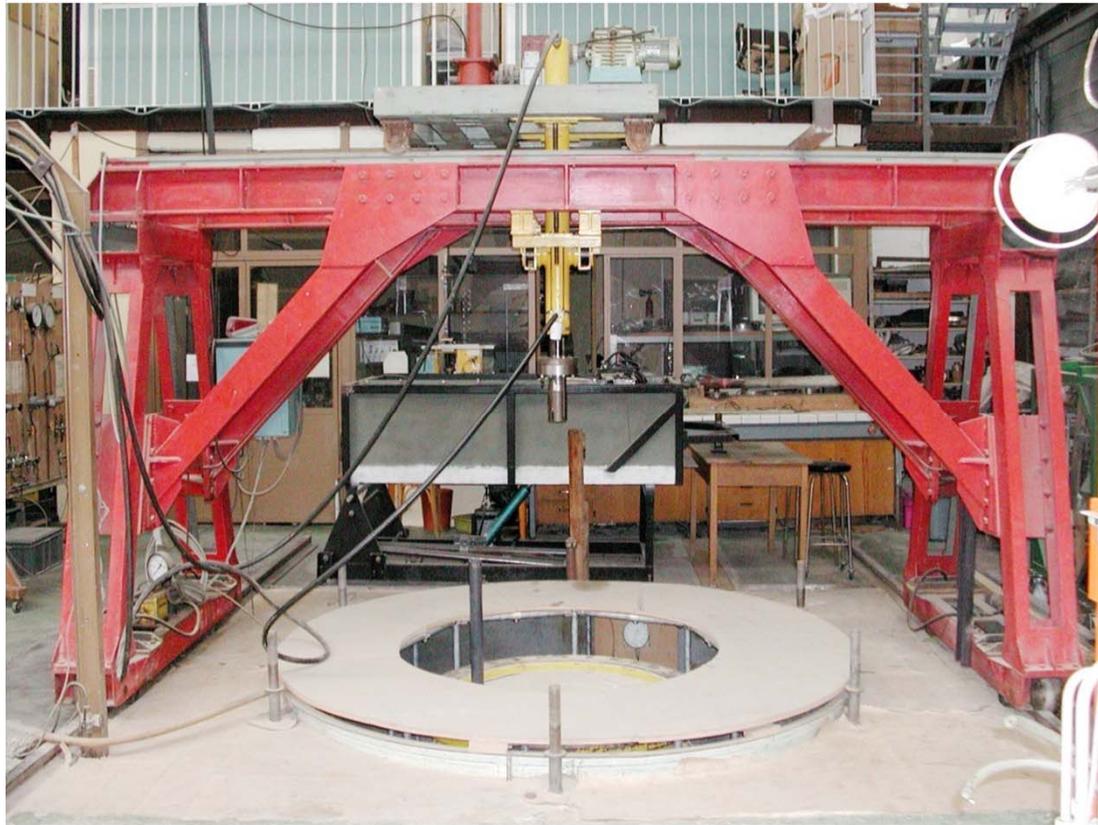


Degradation much worse with bored piles: SOLCYP, Puech et al 2013

**Need for scientific exploration  
of these 'new' phenomena**

Working with Professor Pierre Foray  
2005-2014

# Model experiments with Prof. Pierre Foray



3S-R chamber, temperature & pressure control

Dense NE34 sand; CPT:  $20 < q_c < 25$  MPa

Tests over months under 150 kPa

Up to 36 stress sensors

**Instrumented Mini-ICP**

Foray, Tsuha, Silva M, Jardine & Yang Z.X. (2010) - ICPMG, Zurich

# Mini-ICP model pile

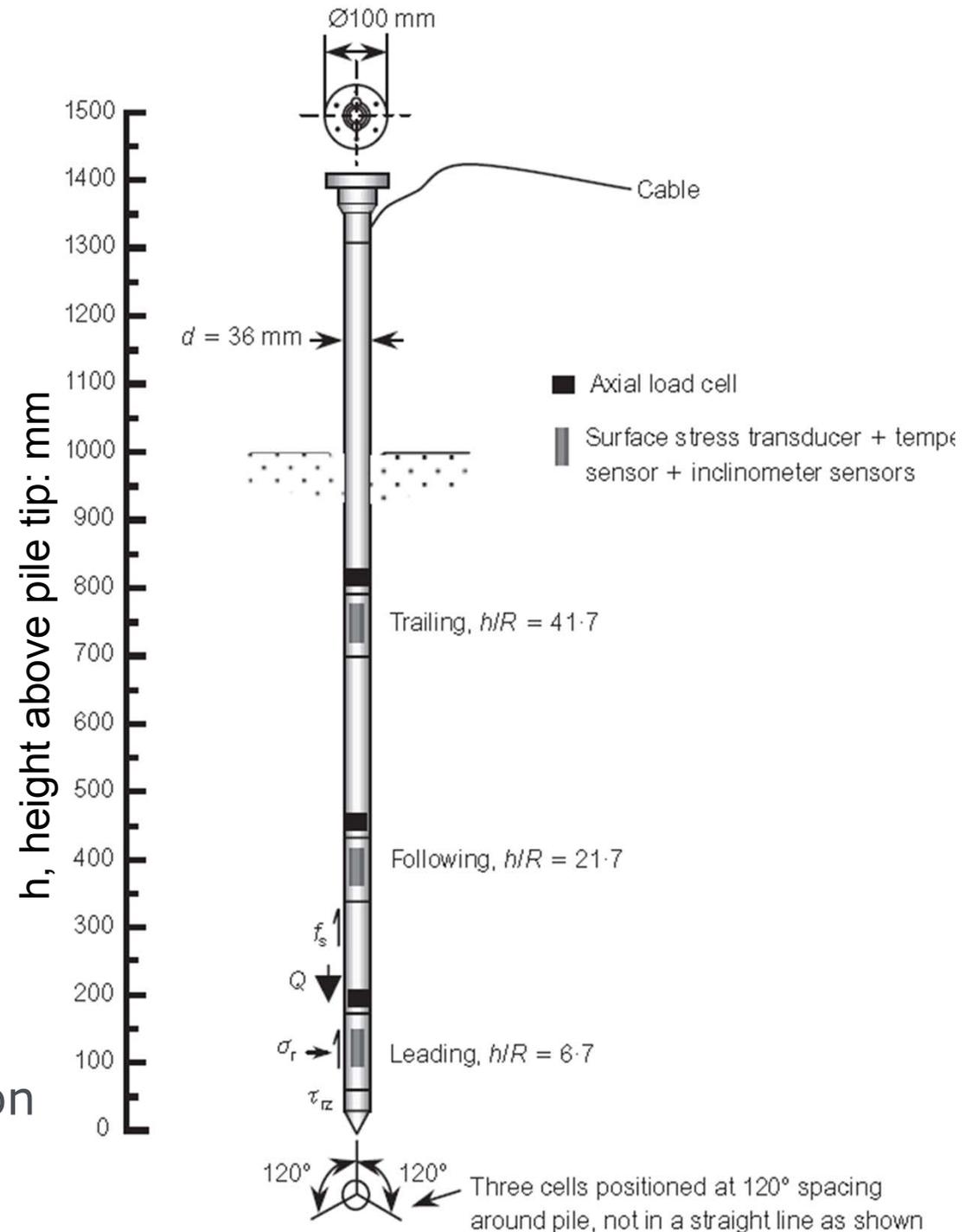
Stainless steel: 36mm OD

Cyclic jacking installation

Local measurements at three  $h/R$  levels of:

- Axial load
- Surface  $\tau_{rz}$  &  $\sigma_r$
- Plus tip loads etc

Jardine, Zhu, Foray & Dalton  
(2009) Soils & Foundations



# **“Hands-on” with Pierre Foray in the 3S-R laboratory**



# **“Heads-down” – problem solving...**



Working even with a geo-endoscope



## Many successful tests over 2007-2013 main programme



**International team:  
Academics, Post-Doc, PhD, MSc & technicians**



Members from:

Brazil

Chile

China

France

Italy

Tanzania

United Kingdom

## **What did we find?**

Distributions of  $\sigma'_r$   $\sigma'_z$  &  $\sigma_\theta$  around piles

Key to modelling ageing, cyclic response,  
group effects..

**Supported by IC-Grenoble laboratory element  
& particle scale studies**

# Installation $\sigma'_r$ trends in sand mass:

1000s data contoured

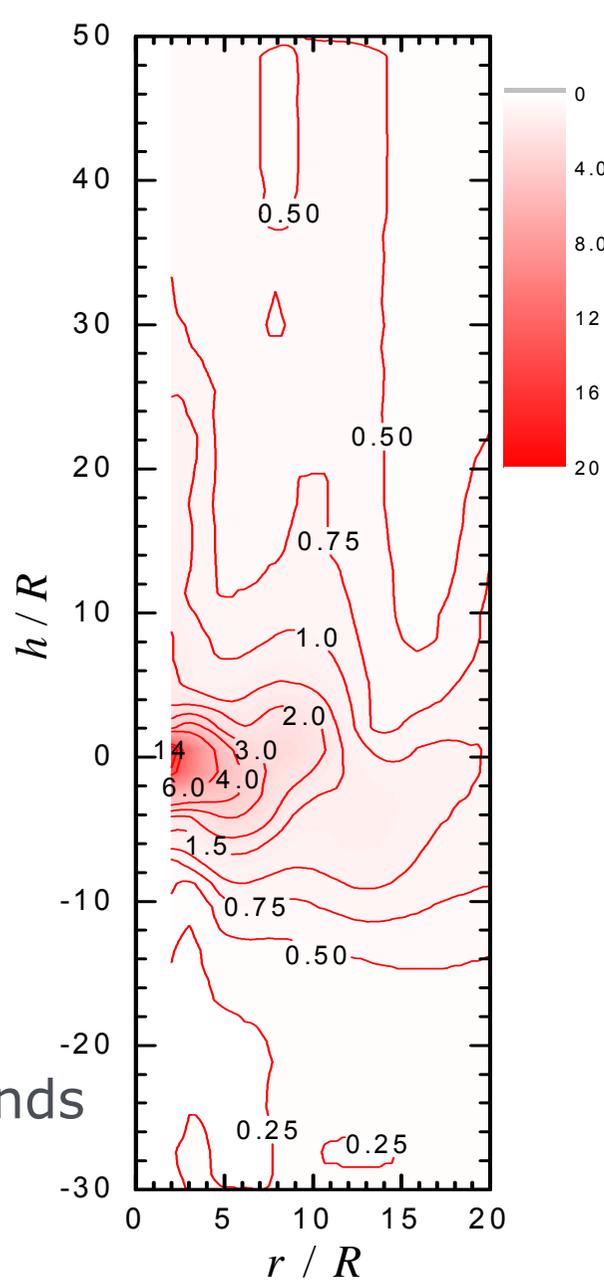
$$\sigma_r/q_c = f(h/R, r/R, \sigma_{z0})$$

Intense tip concentration  
Unloading above tip

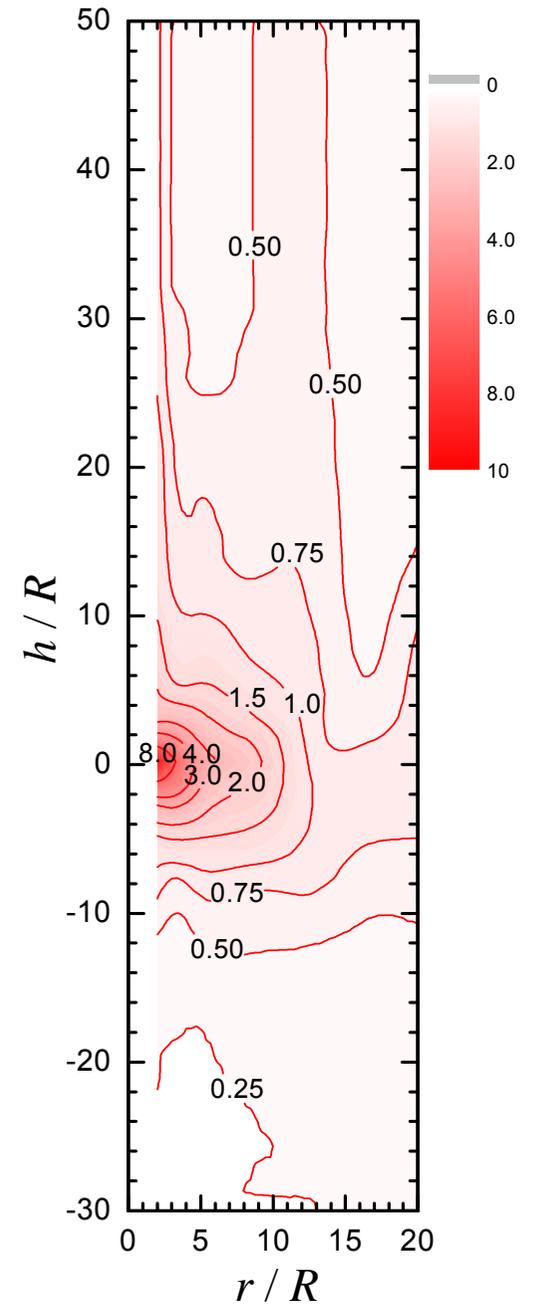
Sharp changes over each jacking cycle

Corresponding  $\sigma_z$  &  $\sigma_\theta$  trends

Jardine, Zhu, Foray & Yang 2013  
Geotechnique

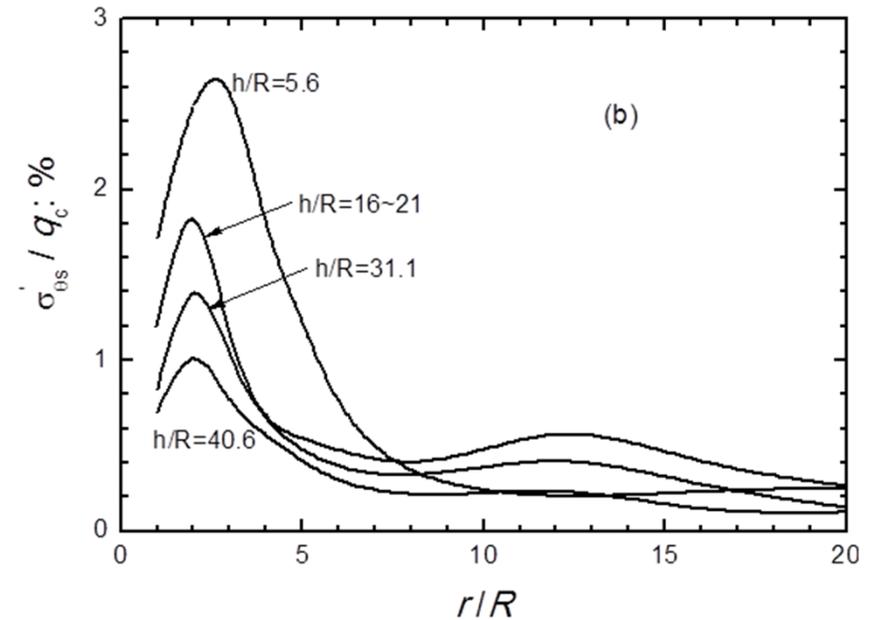
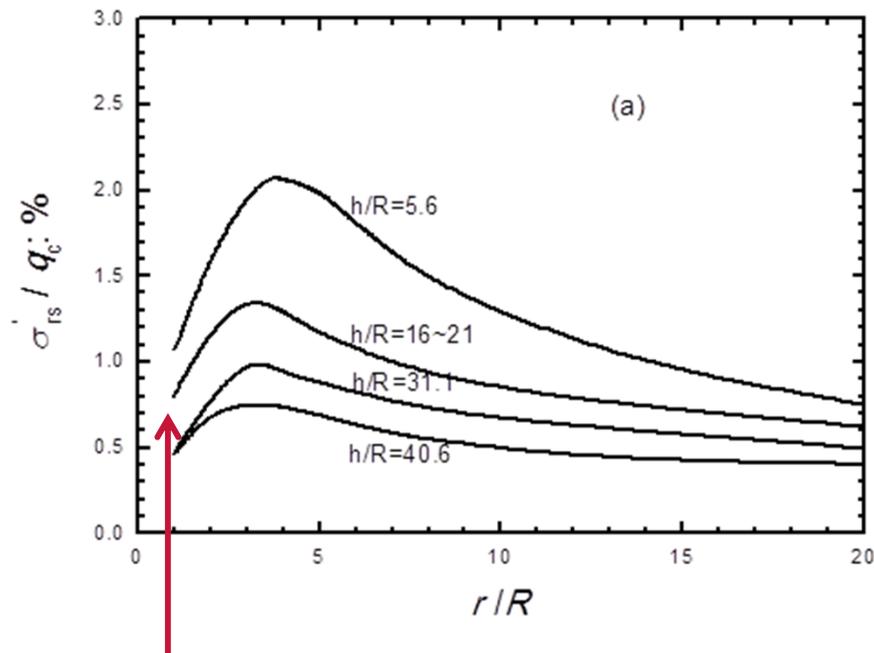


End of push



End of pause

## Radial profiles of $\sigma'_r/q_c$ and $\sigma'_\theta/q_c$ shortly after installation



Radial stresses measured on pile face – far below installation maxima

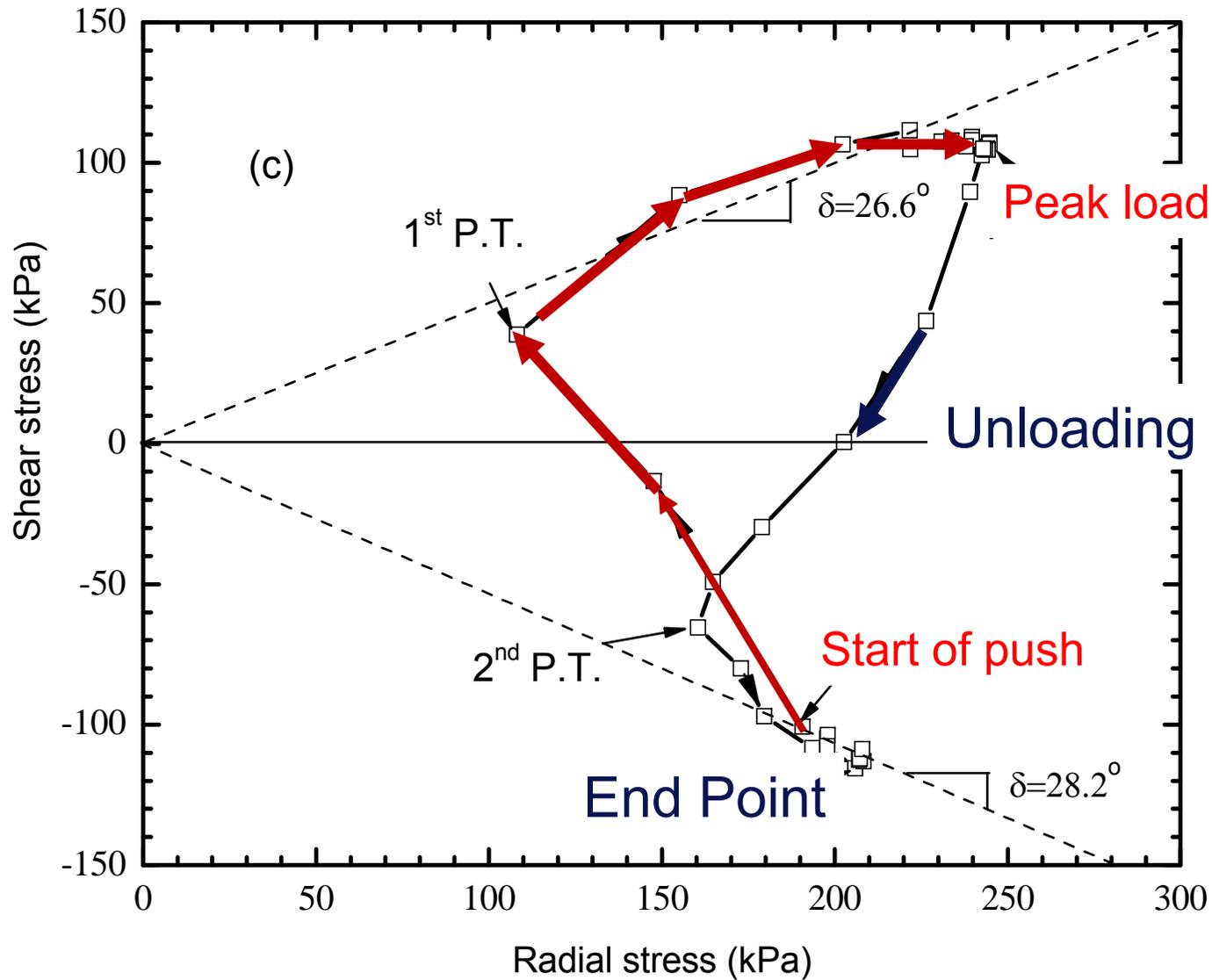
$\sigma_r$  and  $\sigma_\theta$  profiles interlinked, peaks in at  $2 < r/R < 4$

Critical to shaft capacity ageing theories

Compared later to advanced analysis

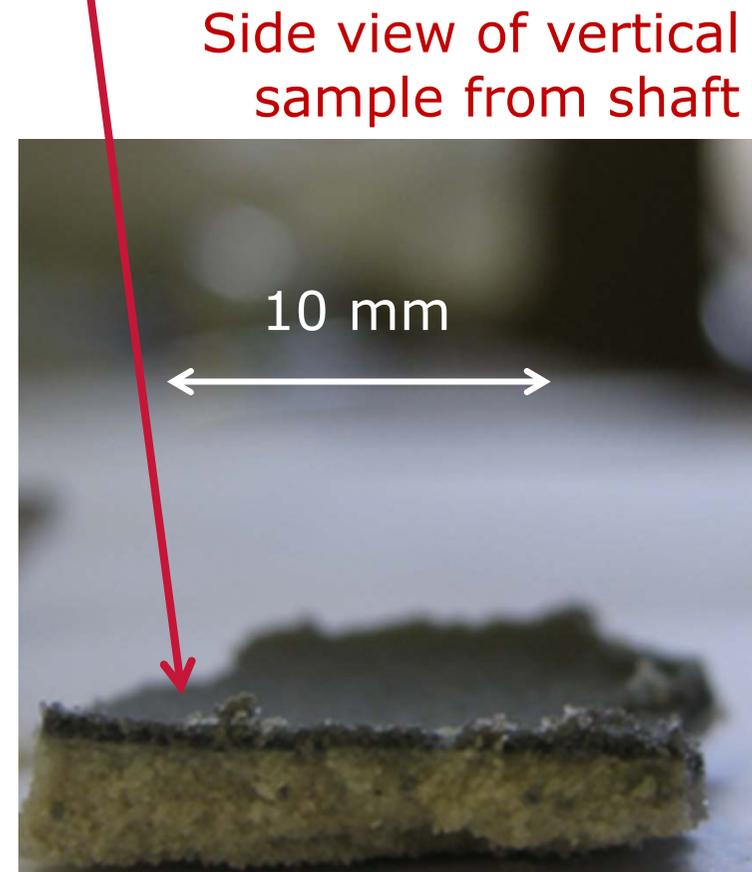
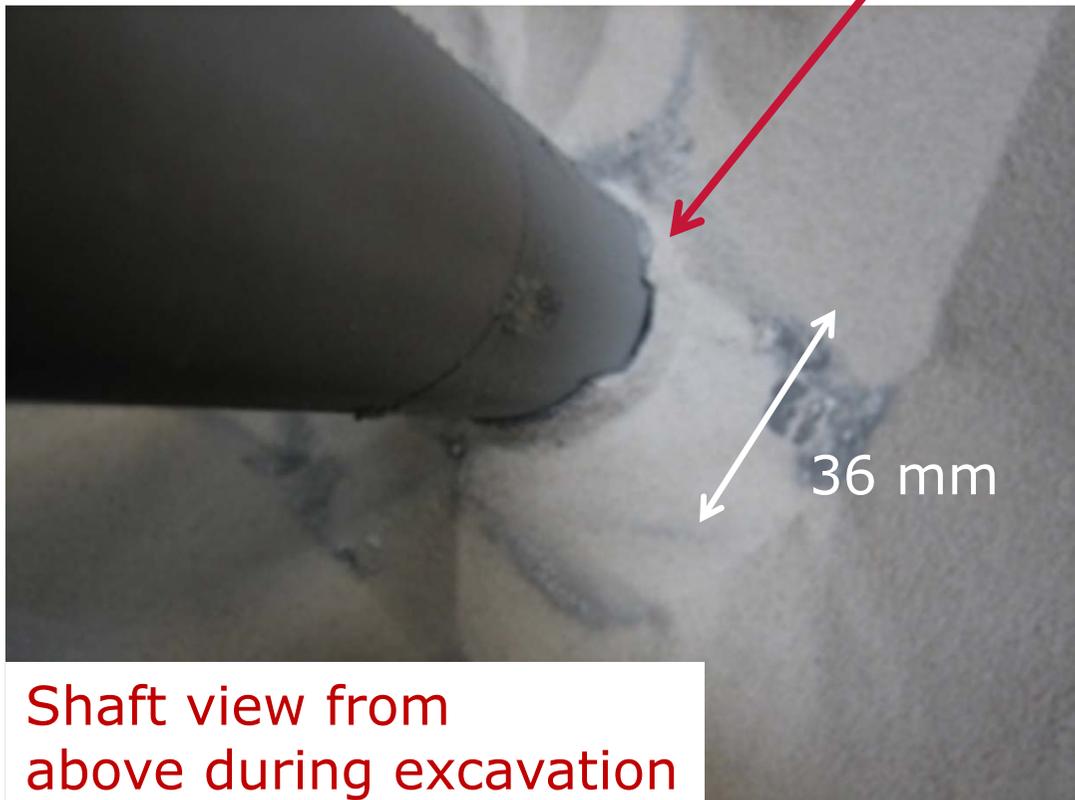
# Local stress paths at Leading pile instrument

One cycle towards end of installation



# Interface shear zone; Yang, Jardine, Zhu, Foray & Tsuha 2010; Geotechnique

Grey dense fractured shear zone 'crust'  
0.5-1.5mm thick, growing with h  
Not present if  $q_c < 6$  MPa



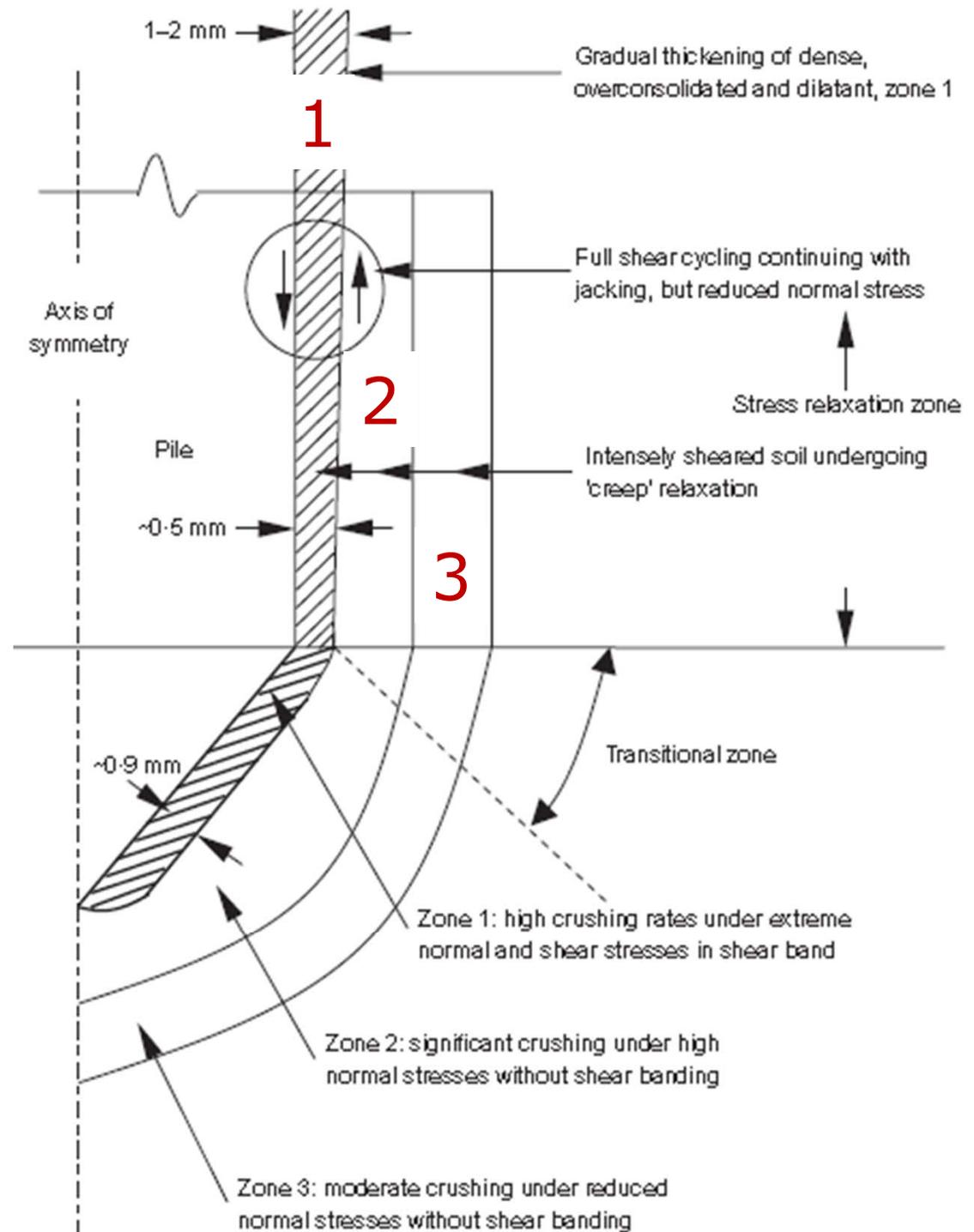
# Breakage Zones 1, 2 & 3

Breakage starts under tip  
 $\sigma'_v > 20$  MPa

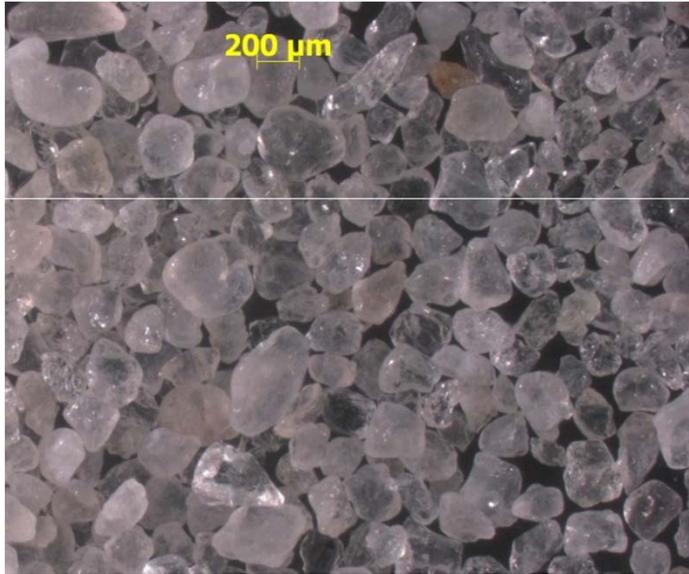
Fractured sand displaced & spread over shaft: **Zone 1**

Further abrasion on shaft

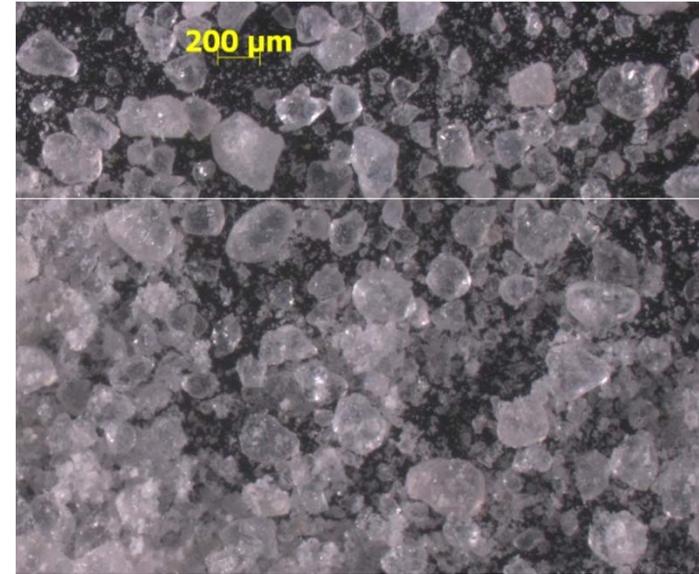
Partial fracturing in outer  
**Zones 2 & 3**



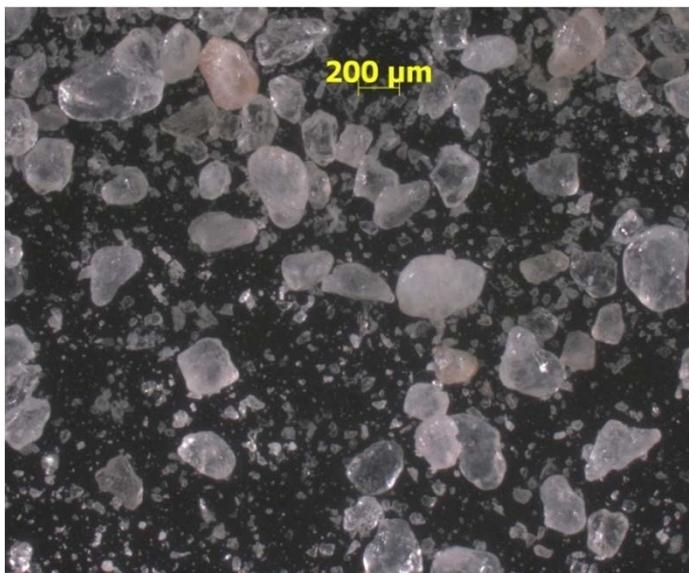
# Micro analysis of progressive grain crushing



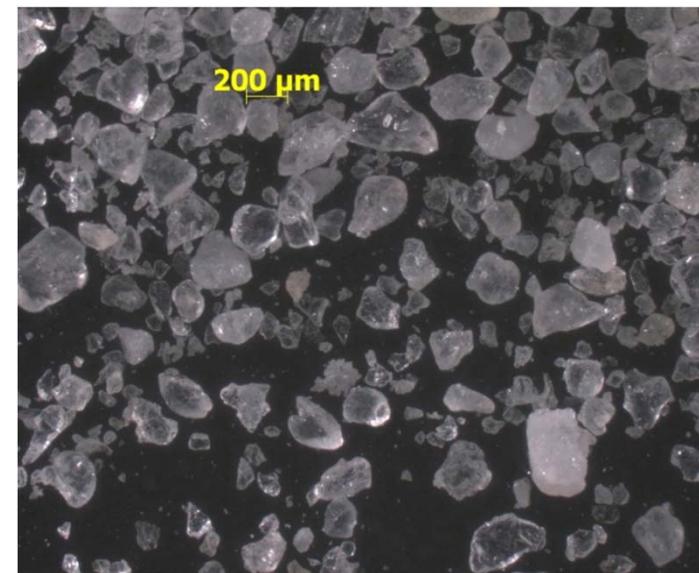
(a) Fresh



(b) Zone 1



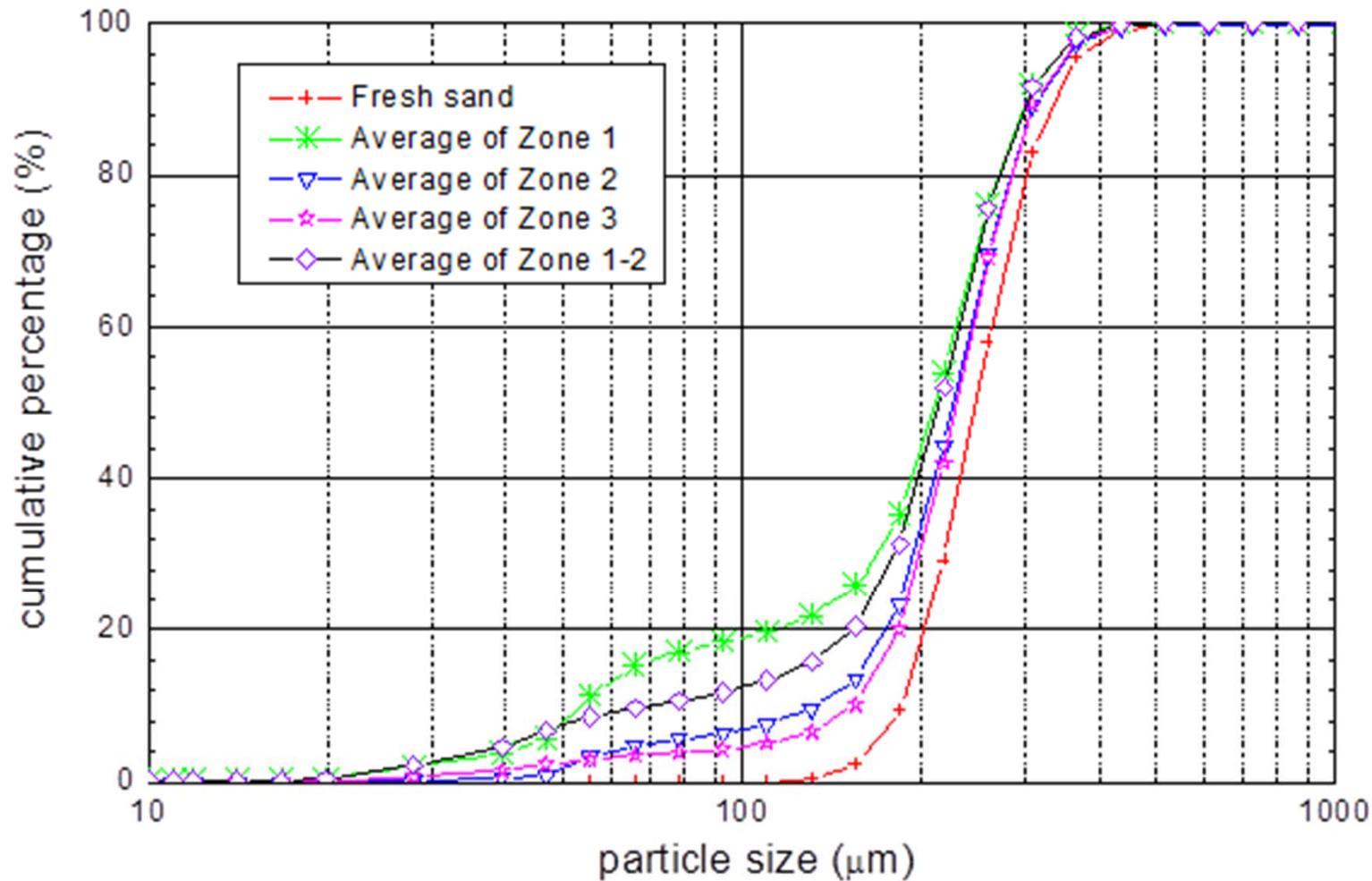
(c) Zone 2



(d) Zone 3

# Qic-Pic laser analyses of small samples:

Progression from **fresh sand** to **Zone 1 'crust'**



Breakage most severe in **Zone 1**, less in **Zones 2 & 3**

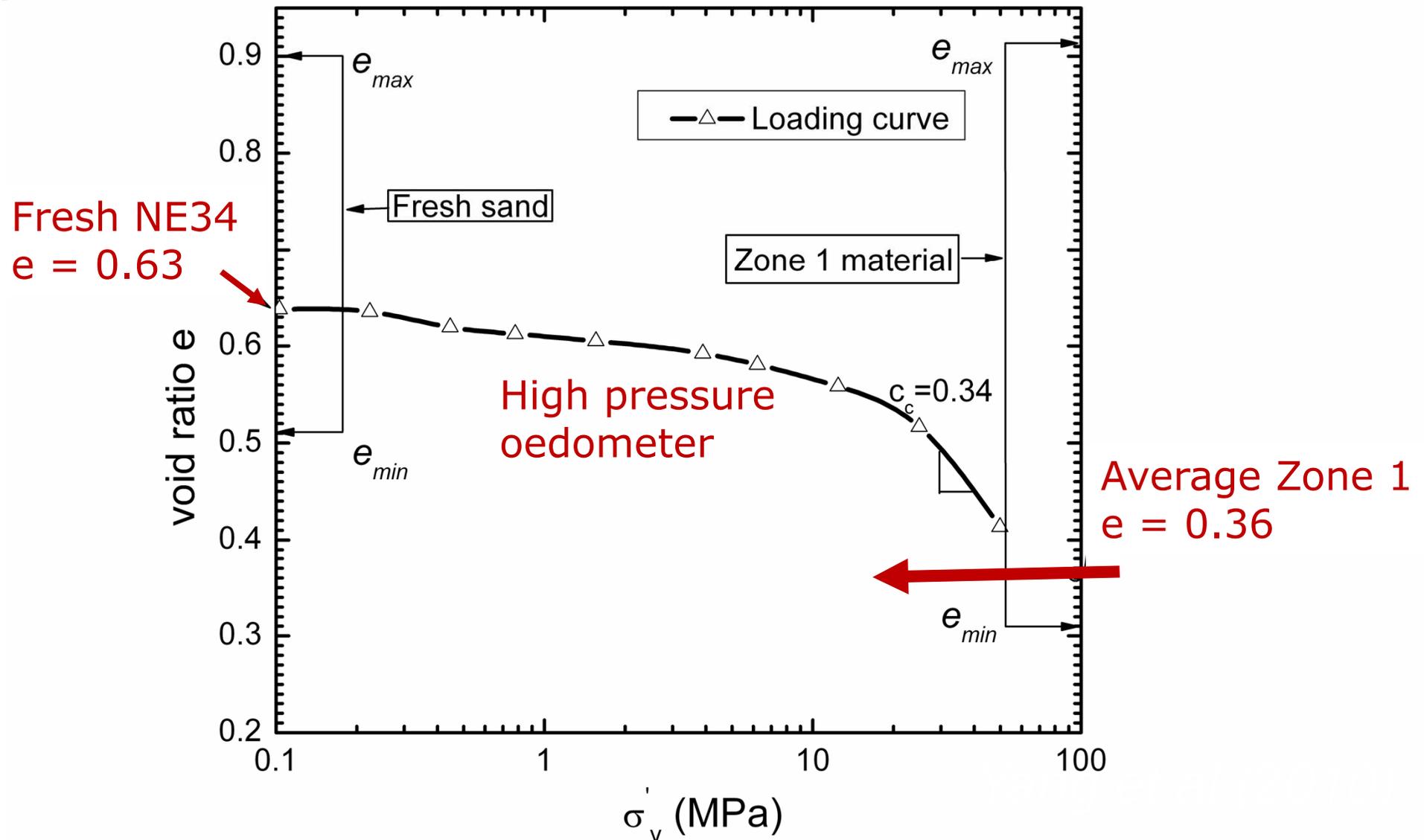
## **Related laboratory tests at Imperial College**

Matching pile conditions in lab tests

Oedometer, interface ring-shear,  
high-to-low pressure stress path  
& cyclic experiments

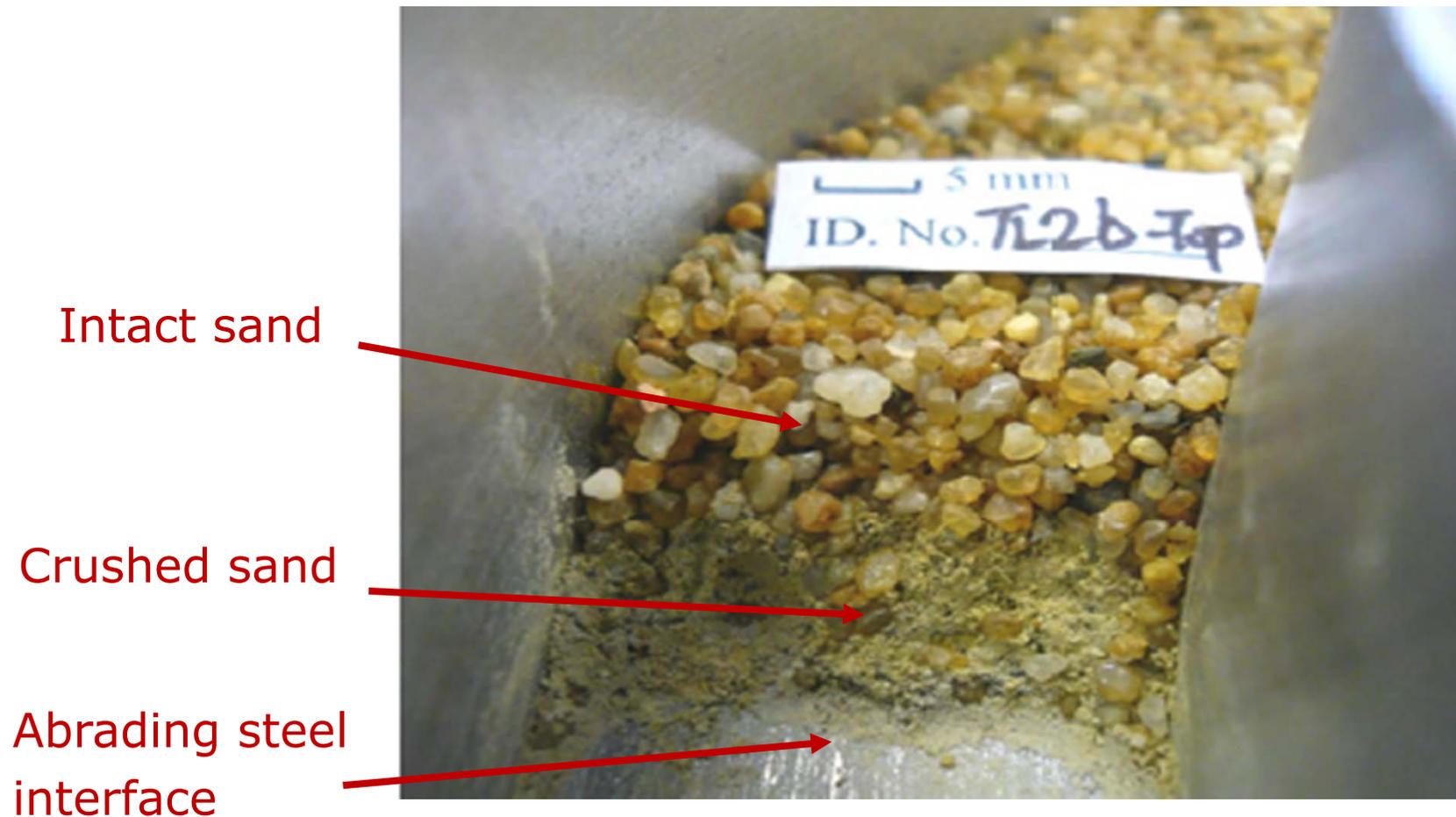
# High pressure oedometer compared to Zone 1

Void ratios, limits & sand states



# Replicating shear zones: 'Bishop' ring-shear interface tests

Coarse example of sands sheared against steel for metres  
 $\sigma'_n$  up to 800 kPa; Ho et al 2011



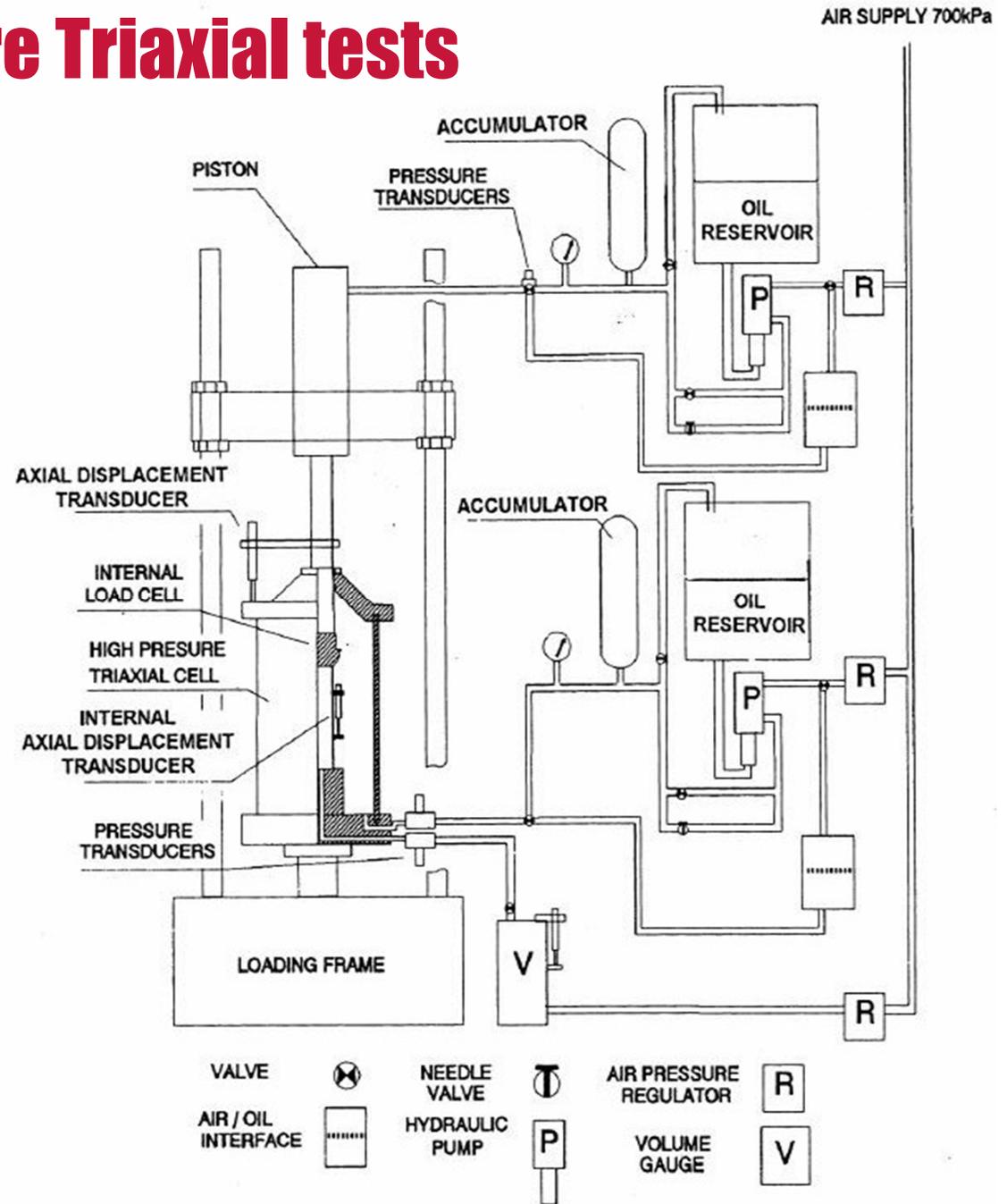
Wide range of sands: different trends to direct shear interface tests

# High-to-Low Pressure Triaxial tests

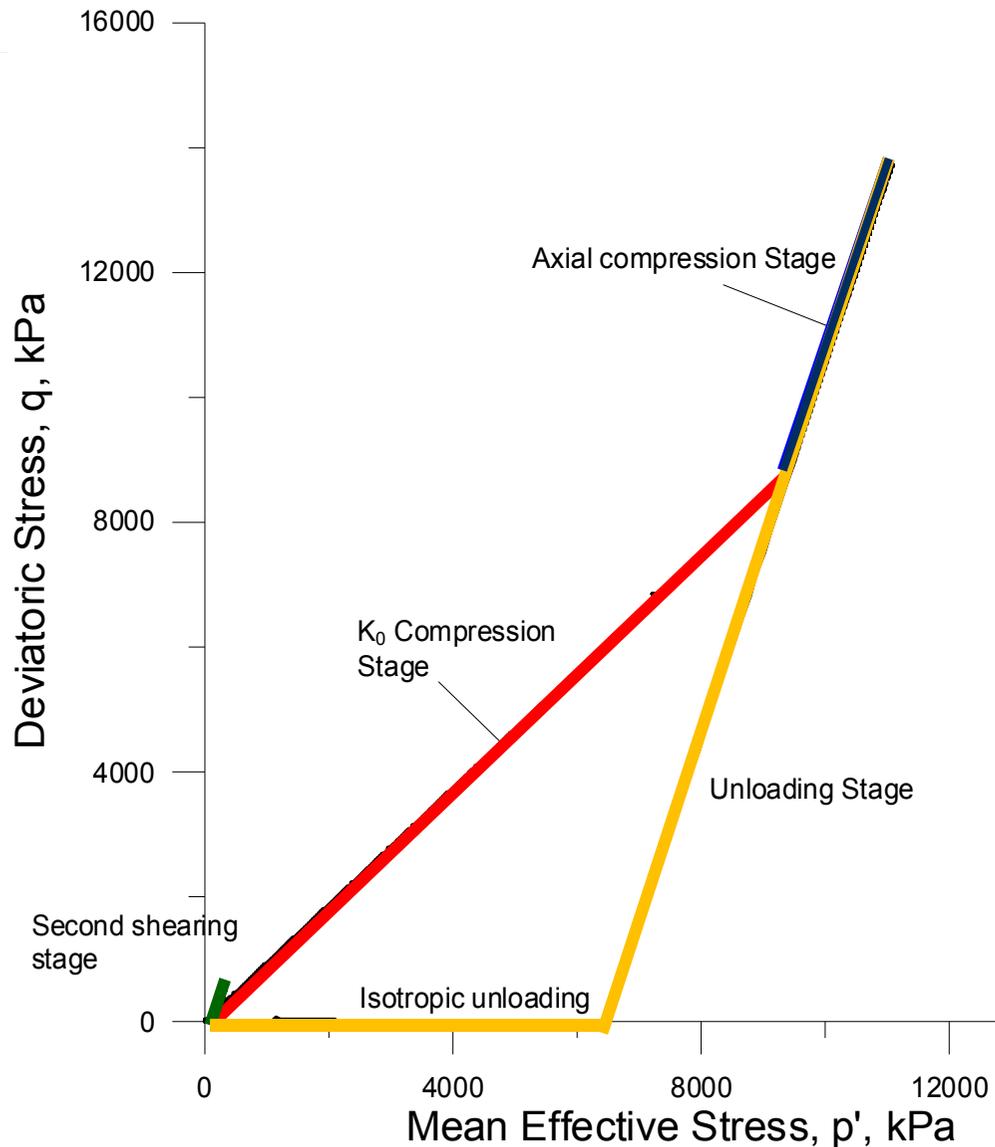
High-to-Low pressures,  
without dismantling &  
changing soil fabric

Matching model pile  
installation stress paths

Altuhafi & Jardine 2011



# High-to-Low pressure stress-path tests



$K_0$  compression: tip advancing from above

Active shearing: tip arrival with  $\sigma'_v > 20\text{MPa}$

Unloading, tip advancing to greater depth

Re-shearing, in compression or extension at high 'OCR'

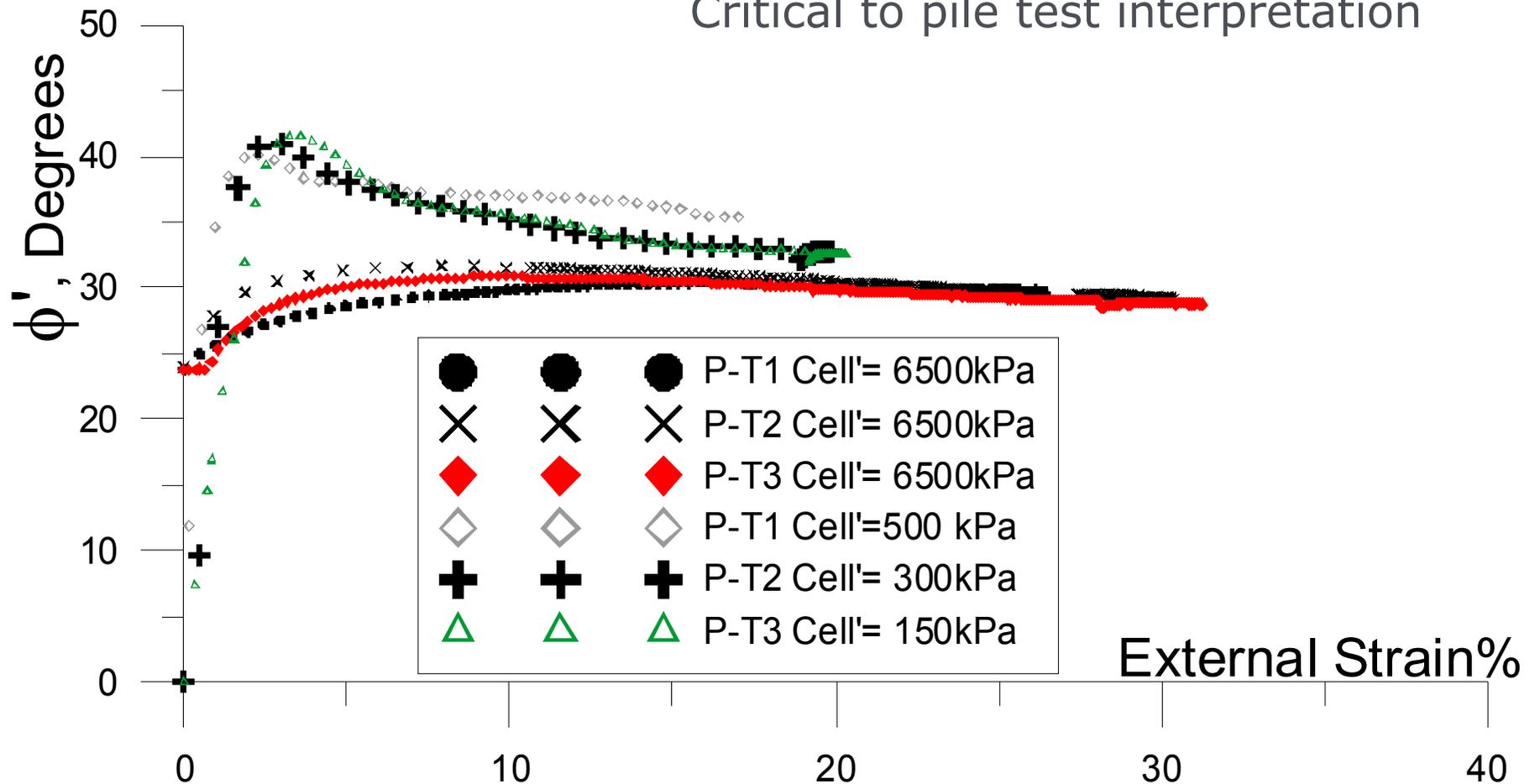
# Effects on angle of shearing resistance?

High pressure 1<sup>st</sup> shearing:

Ductile response low peak  $\phi'$

Low pressure re-shear:

Brittle and much higher peak  $\phi'$   
Critical to pile test interpretation

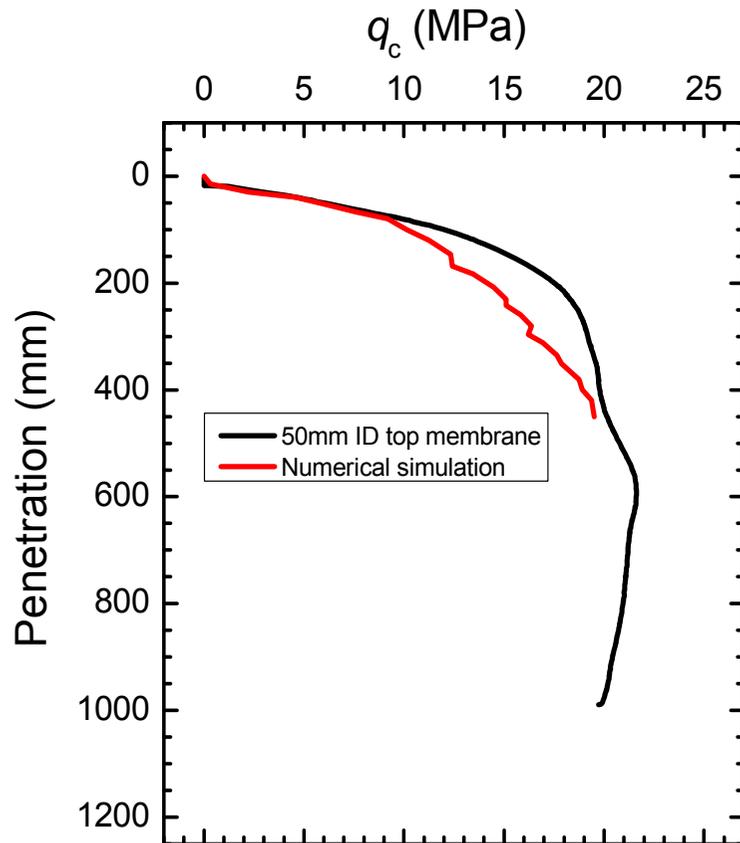


## Ongoing research

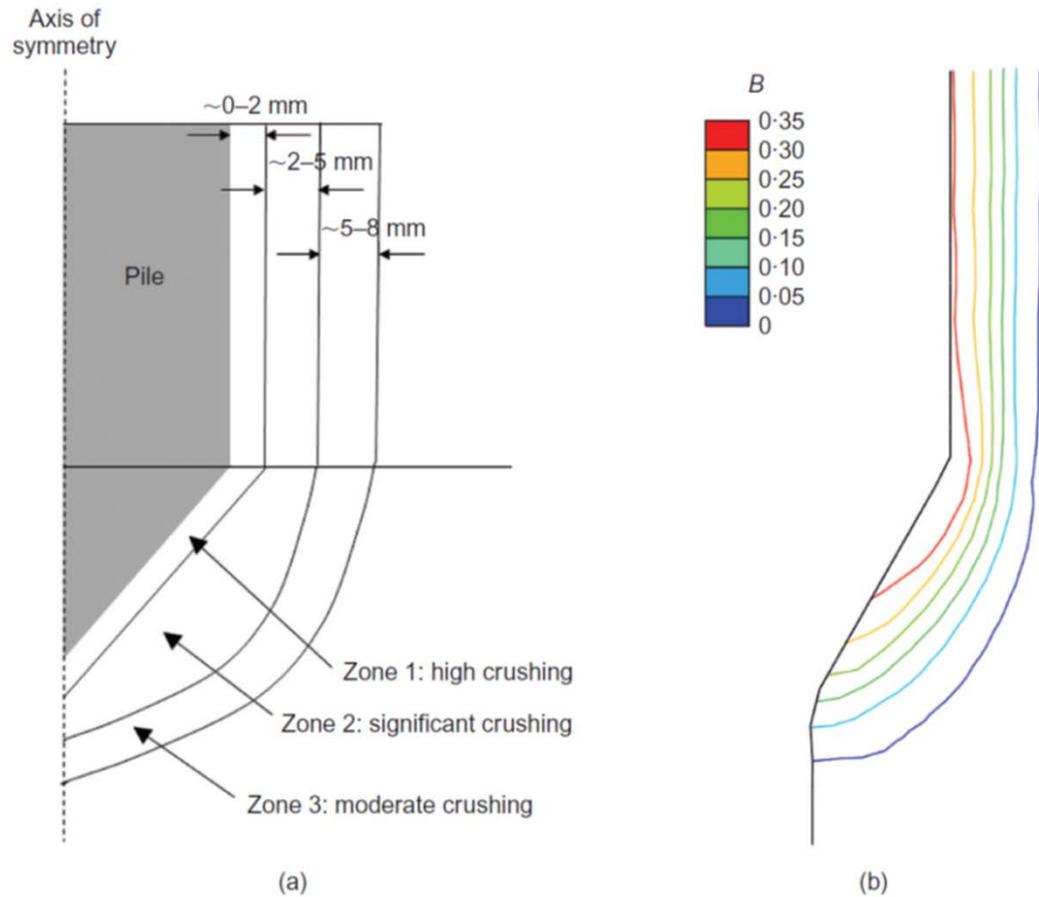
Ageing studies in lab and field  
Rimoy, Silva, Jardine, **Foray**, Yang, Zhu & Tsuha (2015)  
Under Review, Geotechnique

Simulating crushing and pile installation stresses  
**'ALE' Finite Element method with breakage mechanics:**  
Zhang, Yang, Nguyen, Jardine & Einav (2014)  
Geotechnique Letters

# End bearing and breakage: Zhang et al's predictions

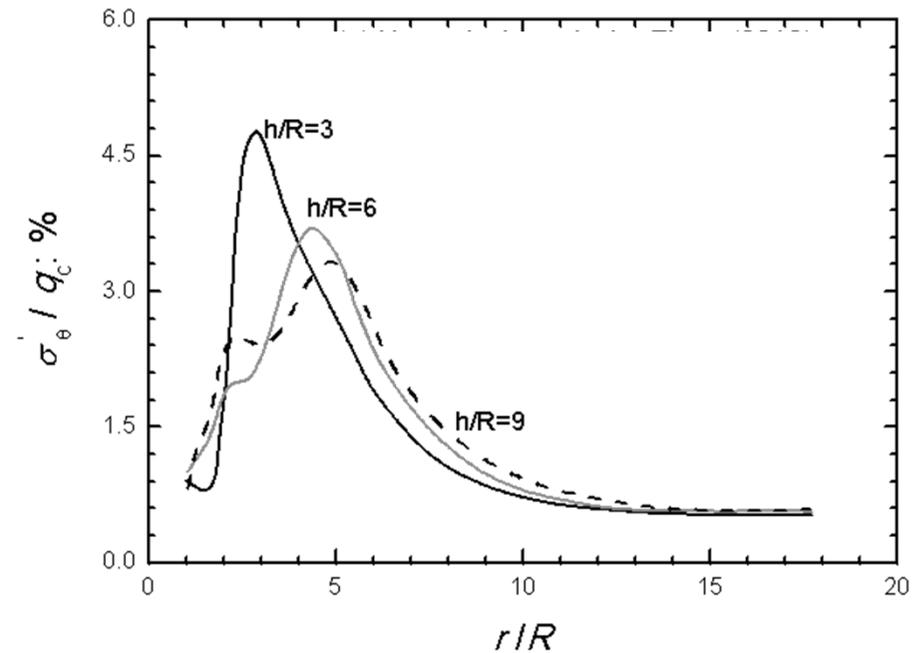
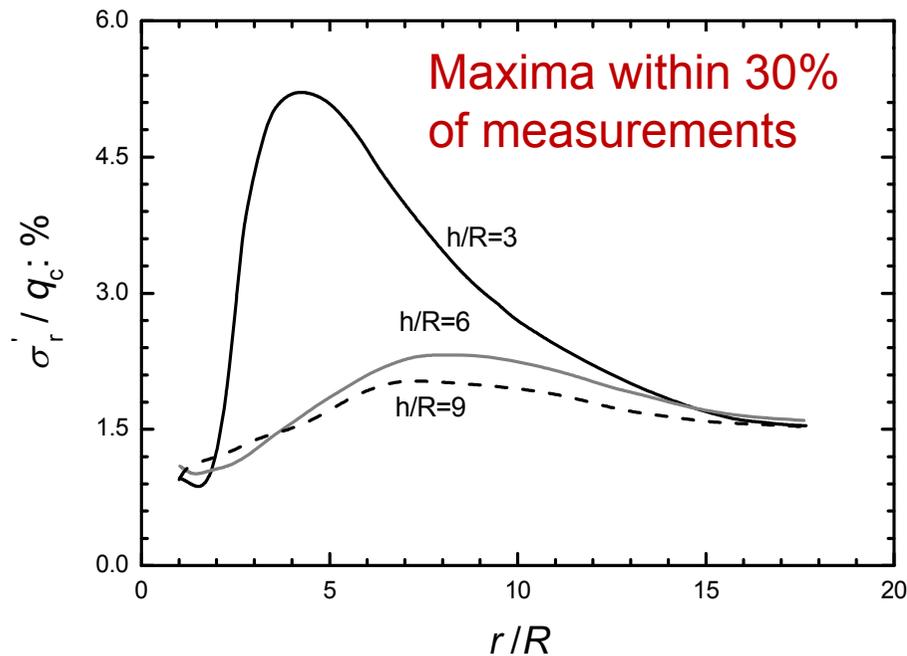


Predicted and measured pile tip stresses  $q_c$



Contours of breakage parameter  $B$ : Fresh sand  $B = 0$ , fully fractured  $B = 1$

# $\sigma'_r/q_c$ and $\sigma'_\theta/q_c$ profiles predicted during installation



Encouraging agreement with **cyclic penetration** model pile tests

But predictions steady at  $h/R > 10$ , while shaft  $\sigma'_r/q_c$  measurements keep falling with  $h/R$

Improve by modelling shaft abrasion & cyclic penetration?

## **Second main theme in 3S-R experiments**

Cyclic axial loading

**Model pile lab tests:** similar overall trends to Dunkerque field experiments, new insights

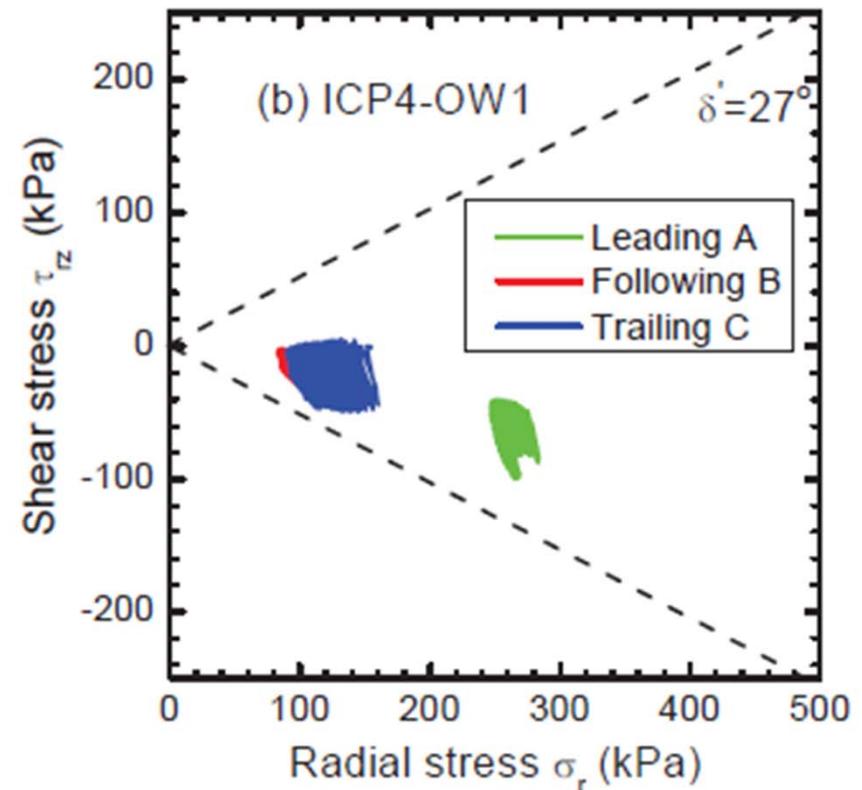
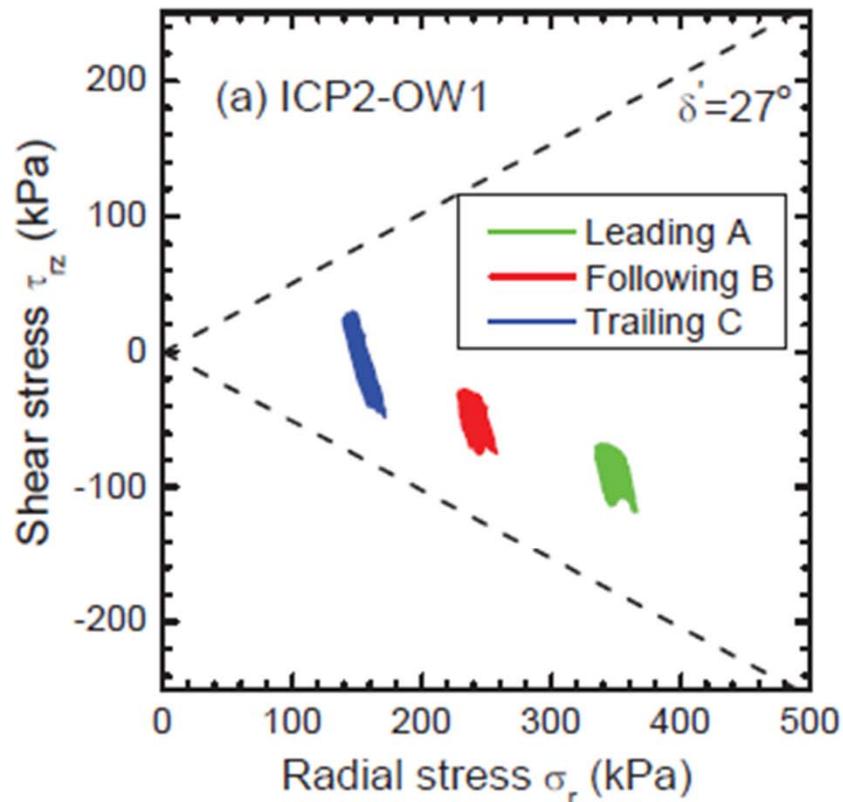
Parallel cyclic **lab element testing**

Integration into practical design

# Stable Mini-ICP cycling: interface stress paths

Load-controlled to  $N > 1000$

Stresses remain within  $Y_2$  shaft capacity rises



Tsuha, Foray, Jardine, Yang, Silva & Rimoy (2012) Soils & Foundations

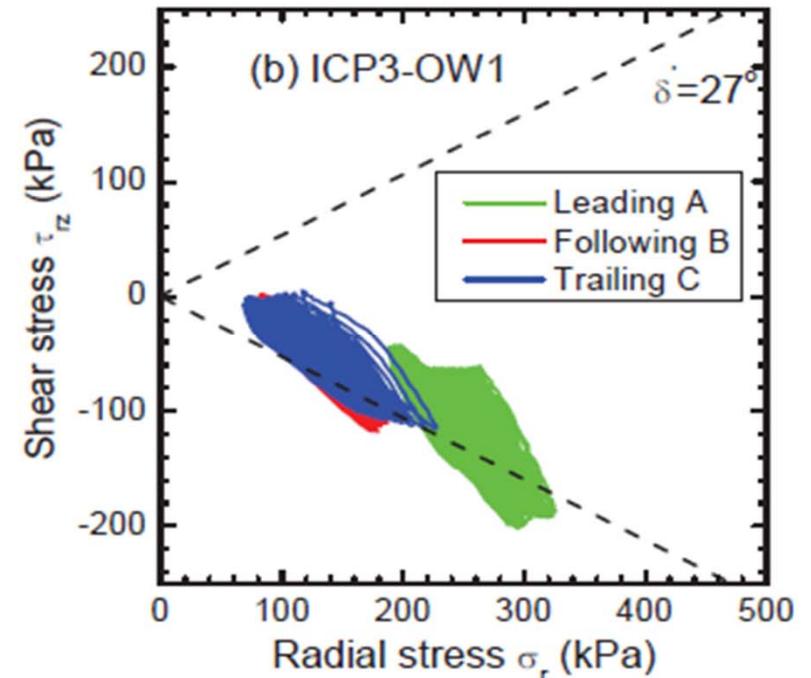
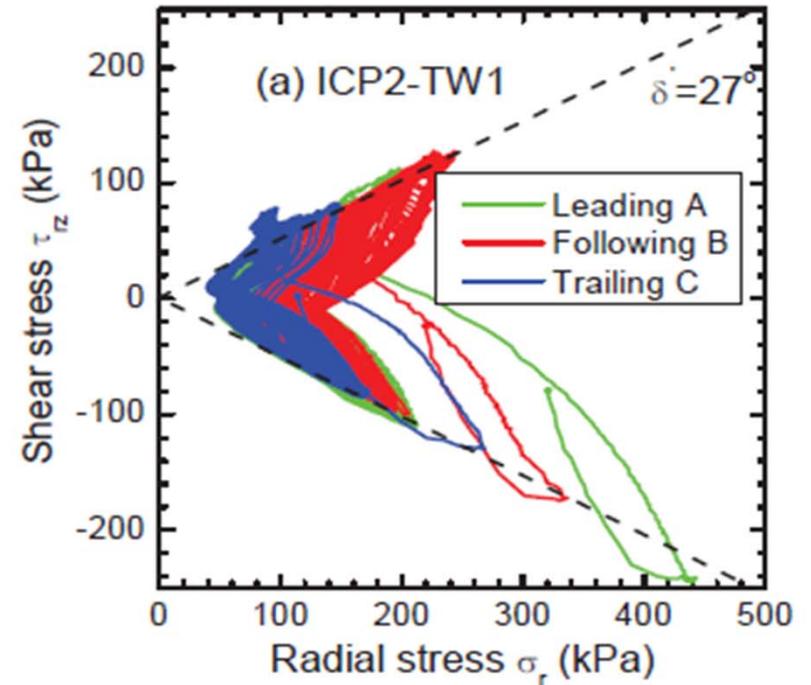
# Unstable stress paths

## Mini ICP tests failing with $N < 100$

Displacement-controlled  
Two-Way tests engage  $Y_3$  and  $Y_4$   
Phase transformation at interface

Load-controlled  
One-Way tests engage  $Y_2$   
Drift towards interface failure

Shaft capacity falls markedly



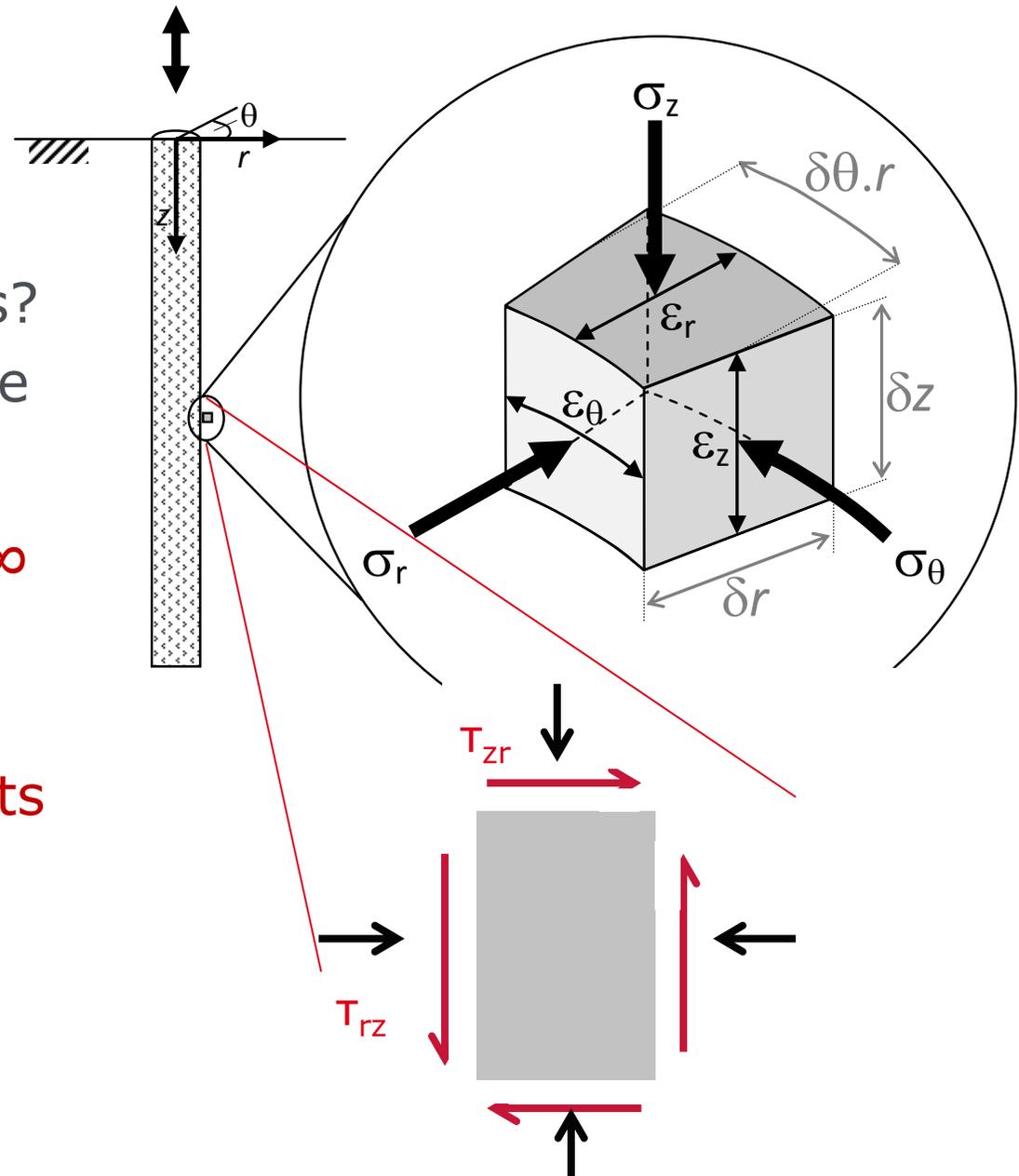
# Matching cyclic conditions in lab element tests

Interface  $\delta\sigma'_r/\delta r = 2G/R$   
Constant Normal Stiffness?  
 $G \neq \text{constant}$ ,  $R = \text{variable}$

Apply undrained  $CNS = \infty$   
in Cyclic Triaxial CTX

Or Simple Shear CSS tests  
Best performed in HCA

Pre-cycling stress path?



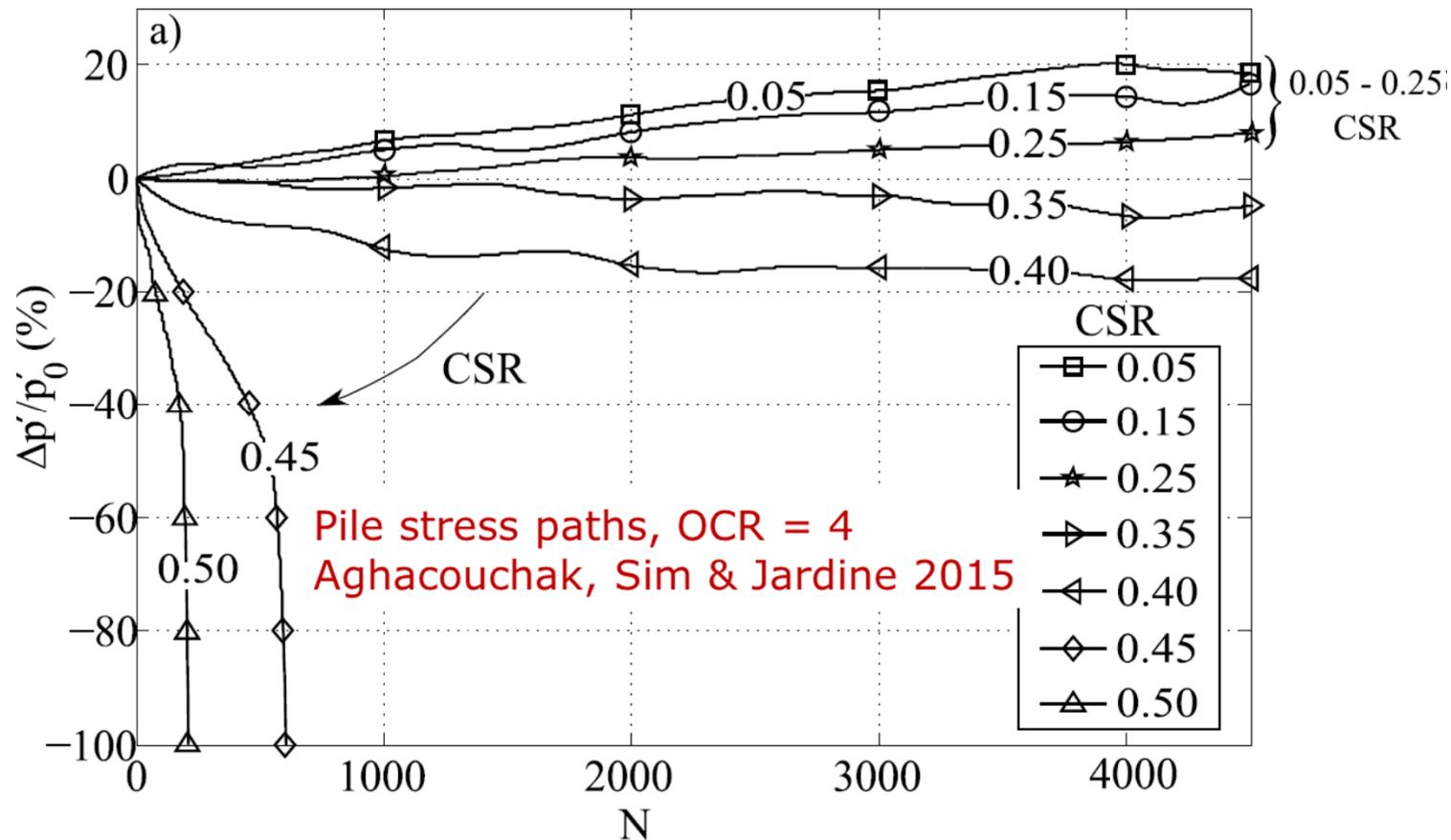
# Undrained cyclic element tests: NE34 & Dunkerque sands

Yielding patterns and  $p'$  drift rates depend on:

CSR =  $q_{\text{cyclic}}/p'$  and N

Shearing mode (TXL or HCA-SS)

OCR & pre-cycling; creep & ageing periods

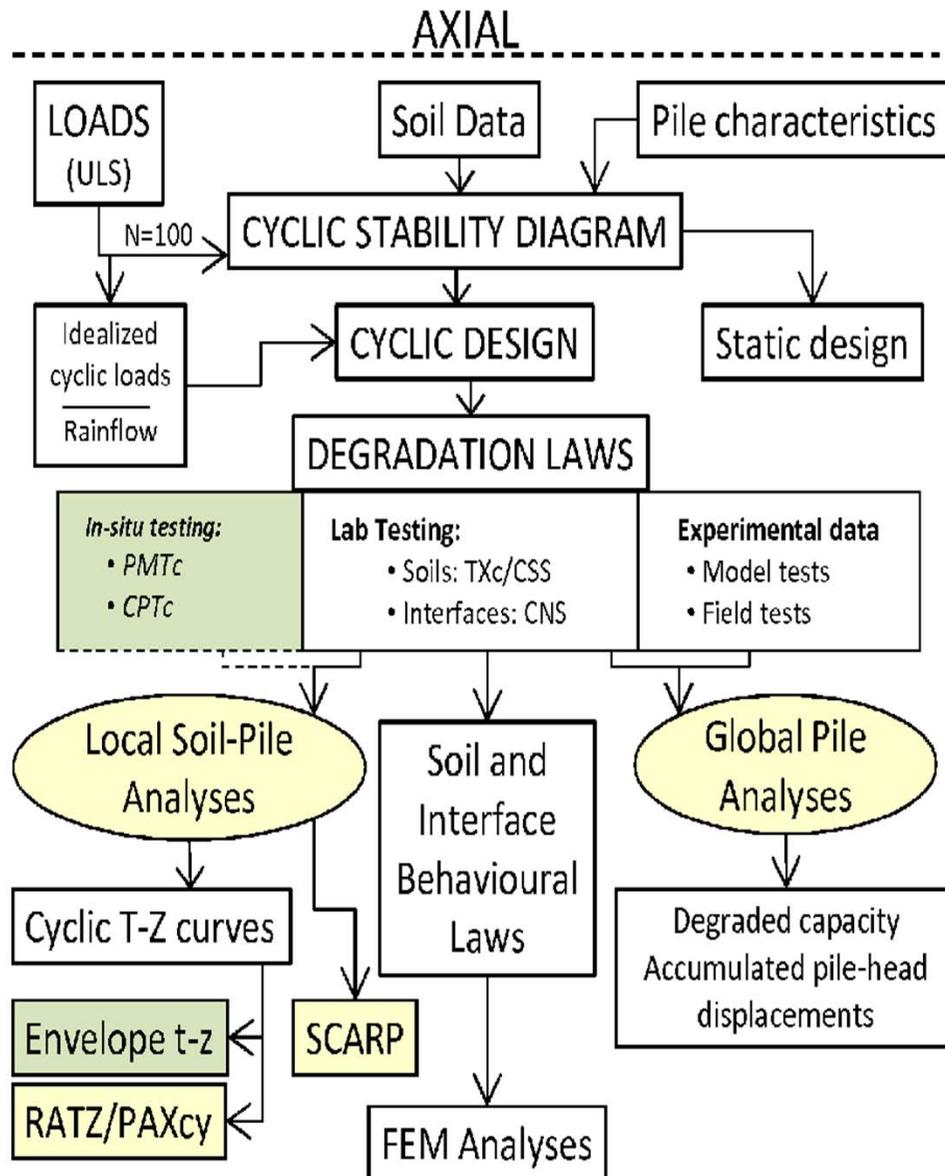


# SOLCYP and applications

# SUT 2012, Paris 2013 workshop

SOLCYP: Puech et al 2013

Jardine, Puech & Anderson 2012  
Anderson, Puech & Jardine 2013



ICP static and cyclic methods for Borkum West II; Merritt et al 2012

Image from [www.heavyliftspecialist.com](http://www.heavyliftspecialist.com)

## Summary

- Challenges posed by field behaviour. New scientific insights needed into ageing & cyclic response
- Critical investigations with Pierre Foray into pile installation stresses, grain-crushing, interface-shear & cyclic behaviour
- Intensively instrumented laboratory model experiments integrated with field, soil element & analytical research
- Results applied in major projects
- Still problems to solve:
  - Effect of scale on driven pile ageing?
  - More field tests needed: at Dunkerque, Larvik or Blessington?
  - Lateral/moment loading – new PISA programme underway: monopiles, tripods, jackets etc

## Professor Pierre Foray 1949-2014



## Other acknowledgments

Sponsors & partners: BP, BRE, CNRS, IFP, EPSRC, Exxon, INPG 3S-R, HSE, Shell, SOLCYP, Total and others

Current and former co-workers: Steve Ackerley, Fatin Altuhafi, Françoise Brucy, Andrew Bond, Fiona Chow, Roger Frank, Itai Einav, Tony Ho, Reiko Kuwano, Barry Lehane, Alain Puech, Siya Rimoy, Matias Silva, Cristina Tsuha, Jamie Standing, Zhongxuan Yang, Bitang Zhu and many others