

## A51 : MONESTIER DE CLERMONT VIADUCT

# FOUNDATIONS OF MONESTIER VIADUCT

- Dominique Quivy
  - Laurent Bastard-Rosset
  - Michel Londez
- VINCI Construction France  
GTM TP Lyon  
Independent expert Mécasol





**GTM TP**  
LYON

# MONESTIER DE CLERMONT VIADUCT



---

MONESTIER DE CLERMONT VIADUCT

- Contracting Authority
- Design and built joint venture
- MECASOL
- VINCI Construction B.E.T.
- STRATES
- PAYSAGE PLUS
- BAUDIN-CHATEAUNEUF



**Les Autoroutes Rhône-Alpes**



**GTM TP Lyon, mandatary**



**Geotechnical engineering**



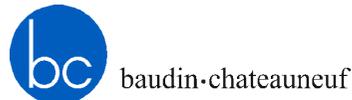
**Civil engineering design office**



**Architect : Jean-Vincent**

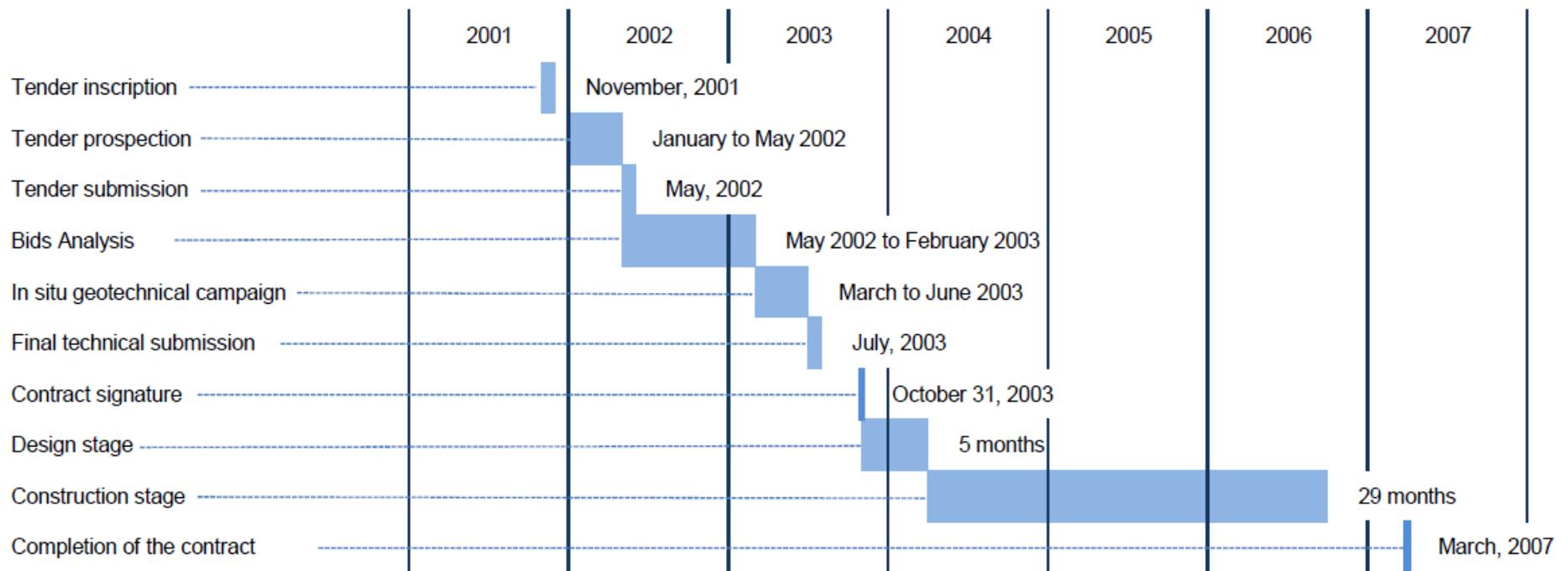


**Berlottier**



**Landscape painter**

**Structural steel Construction**







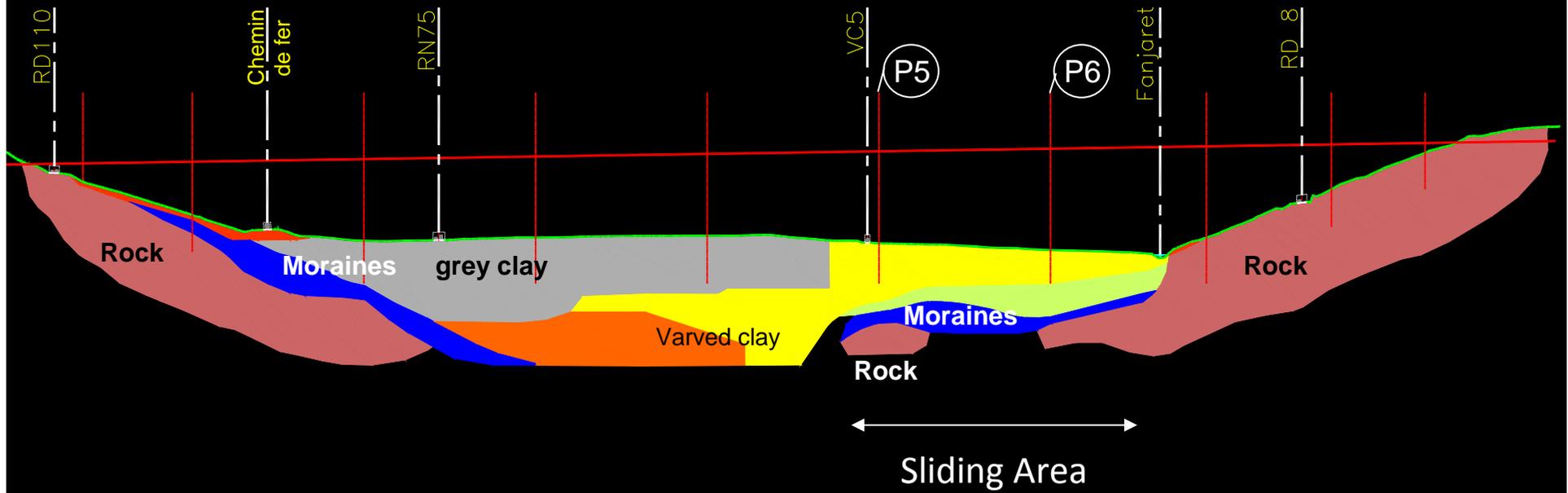
**GTM TP**  
LYON

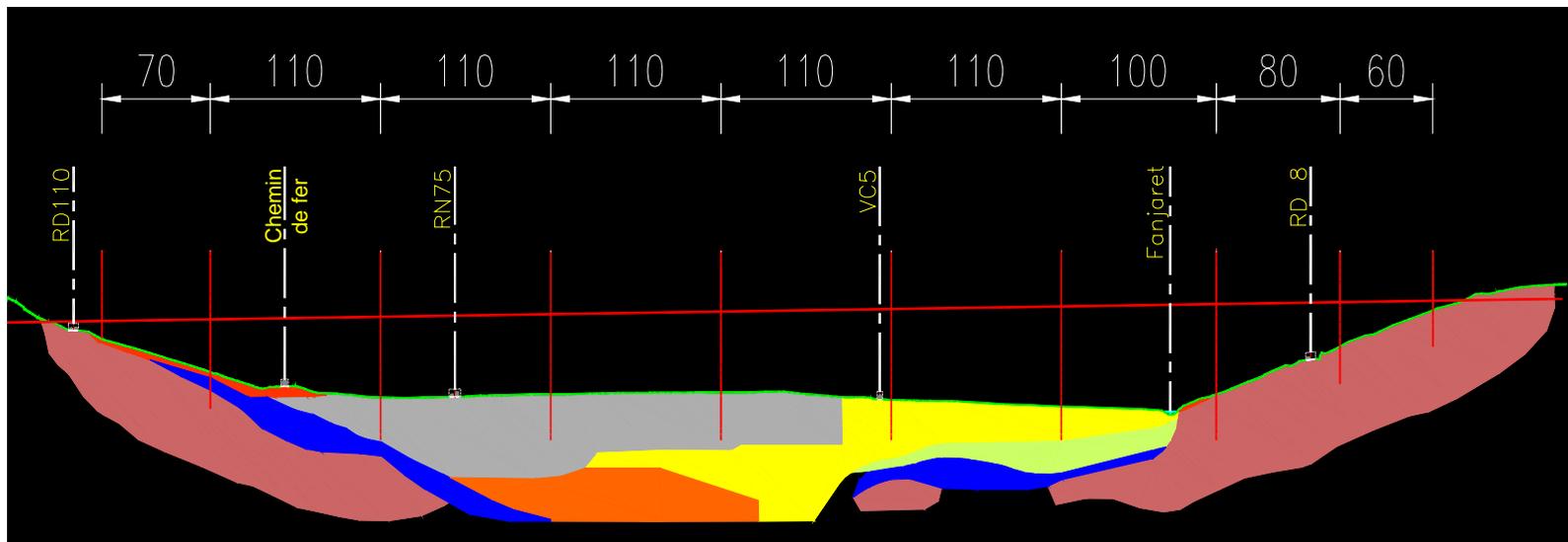
# GEOTECHNICAL ENVIRONMENT

## Michel LONDEZ

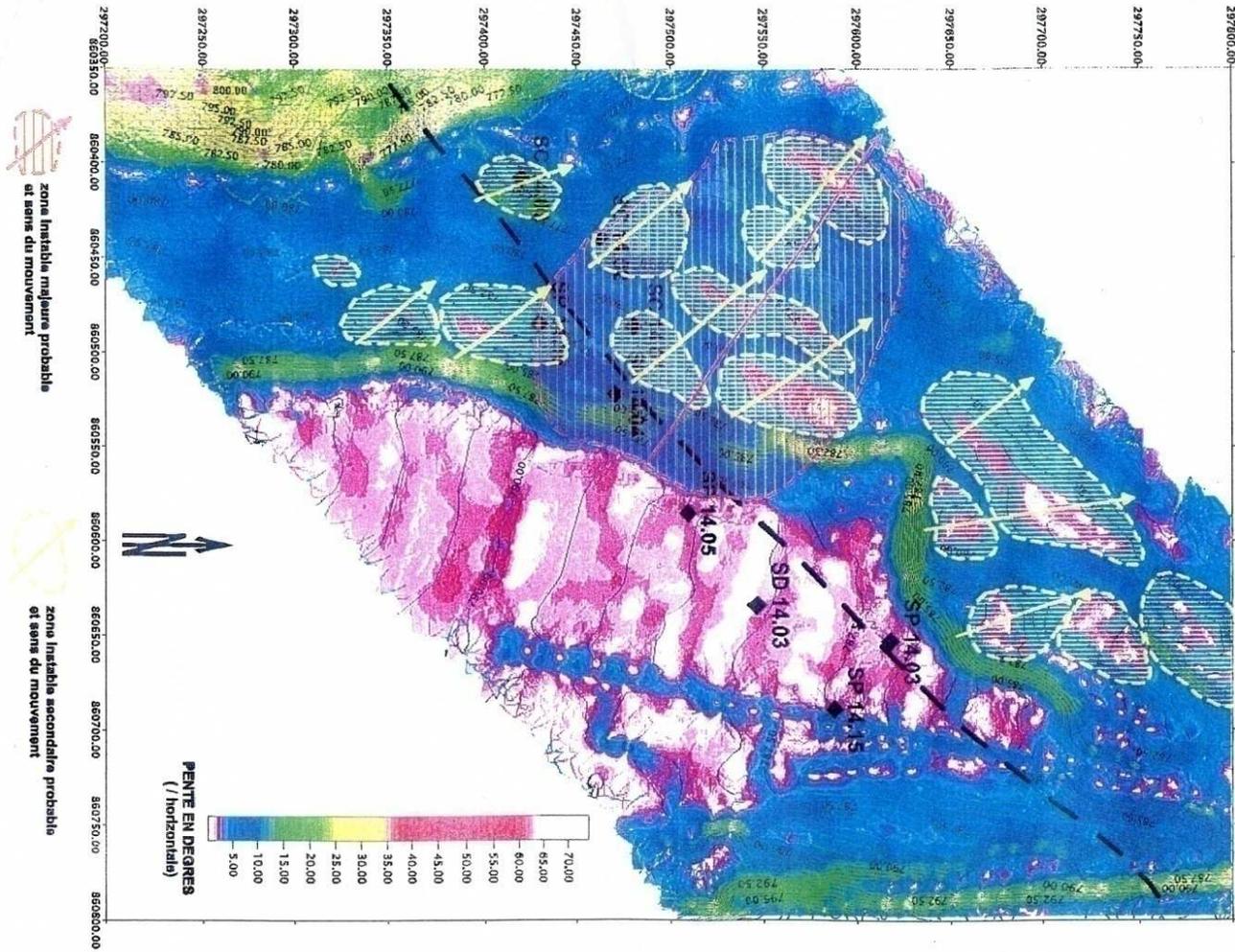


# GEOLOGICAL CROSS SECTION





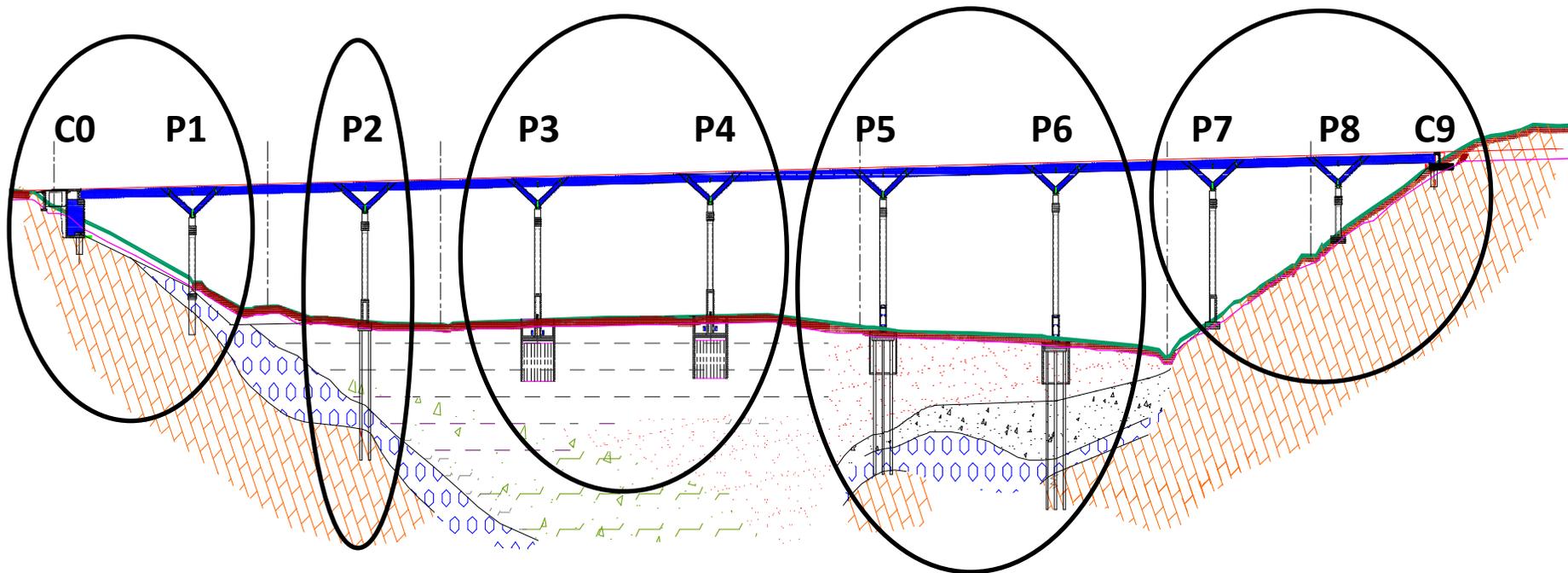
**A51 VIADUC DE MONESTIER**  
**RECHERCHE DES ZONES GLISSEES**  
**CARTOGRAPHIE DES ZONES INSTABLES PROBABLES**  
**1 / 2 000**

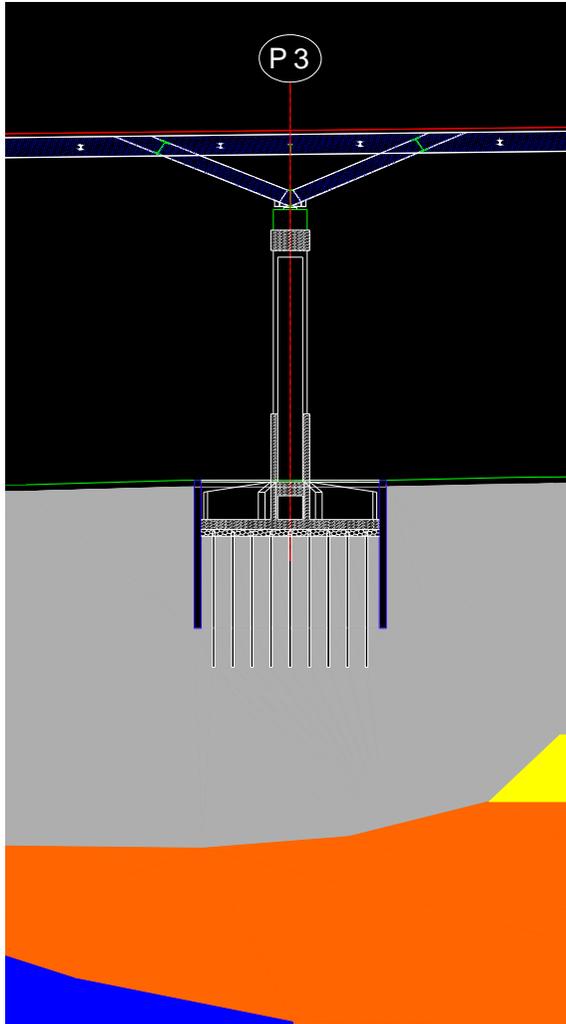




Five different types of foundations :

- C0 & P1 : Large pits (4 m diameter)
- P2 : Concrete piles (1,5 m diameter)
- P3 & P4 : semi-deep Foundations
- P5 & P6 : Piles inside circular diaphragm wall
- P7, P8 & C9 : Spread footing

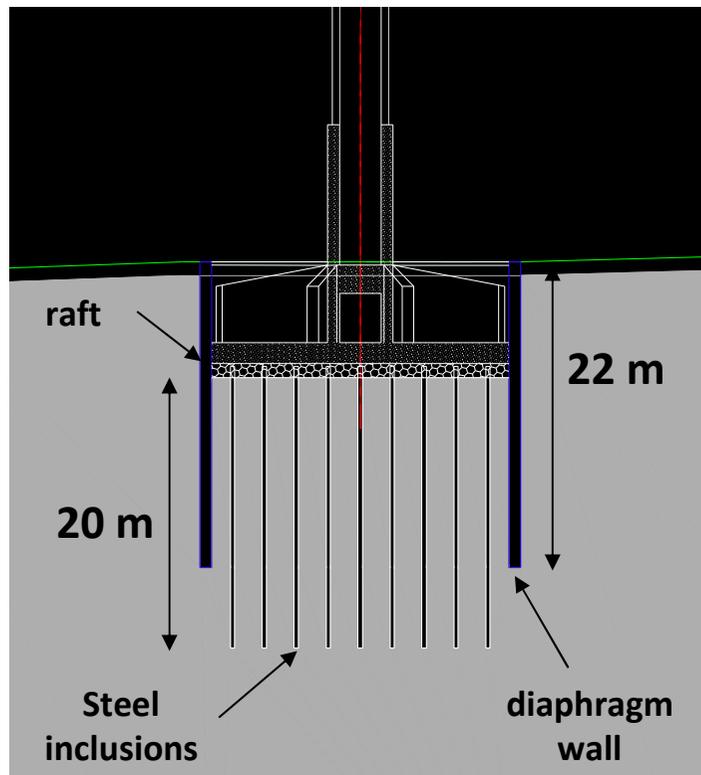
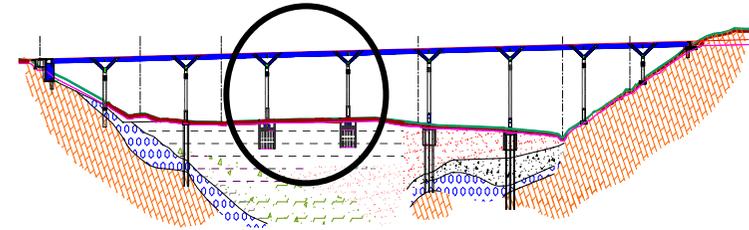




Bellow P3 and P4, varved clay which is water saturated, is present up to 80m deep.

Ground is therefore not stiff enough to carry heavy loads.

The design of the foundations is quite unusual : the principle consists in taking off a quantity of clay equivalent to the load brought by the pier itself (weights of the foundation + pier + deck ).



## P3 FOUNDATION INCLUDES :

- a diaphragm wall (20m diameter and 22m deep).
- 20m long steel profiles (HEA 300) driven into clay
- a 1,50m thick concrete slab, poured above a 1,00m thick gravel layer.
- 80cm thick concrete walls stiffening the structure and allowing transfer of pier load to the diaphragm wall and concrete slab.
- The inside volume (1700m<sup>3</sup>) remains empty except during construction of the pier when it is filled with water.





# P3 & P4 : DIAPHRAGM WALLS REINFORCEMENT AND CONCRETE



# P3 & P4 : STEEL PROFILES DRIVEN INTO CLAY (STAGE 1)



# P3 & P4 : CLAY EXCAVATION INSIDE DIAPHRAGM WALLS



## FINAL PREPARATION OF THE GROUND BEFORE GRAVEL LAYING OPERATIONS AND CUTTING BACK OF STEEL PROFILES



# P3 & P4 : STATE OF THE FOUNDATION JUST BEFORE GRAVEL IS LAY DOWN







**GTM TP**  
LYON

# P3 & P4 : REINFORCEMENT OF CONCRETE SLAS

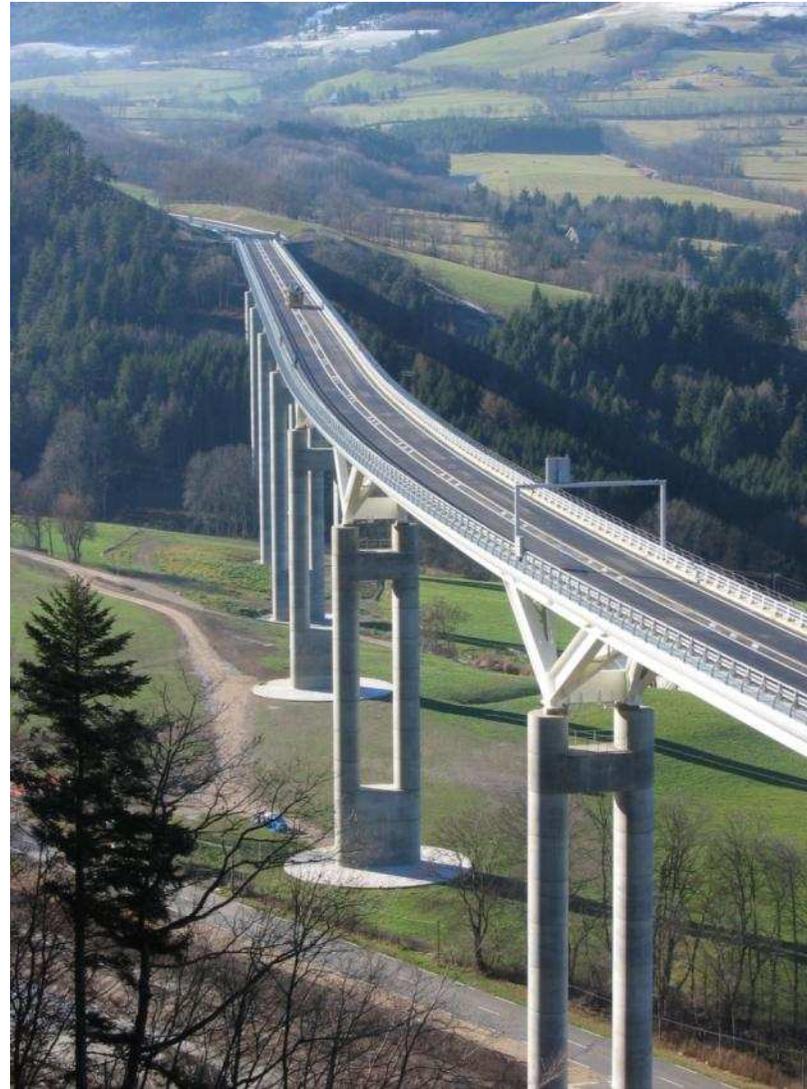




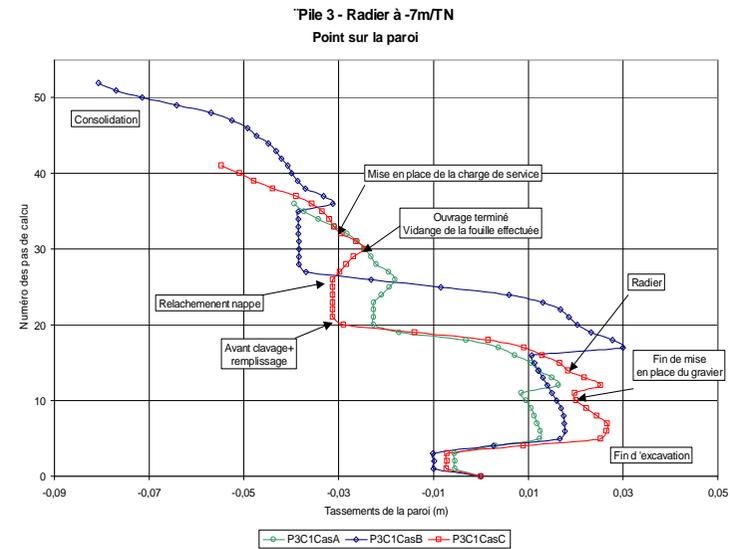
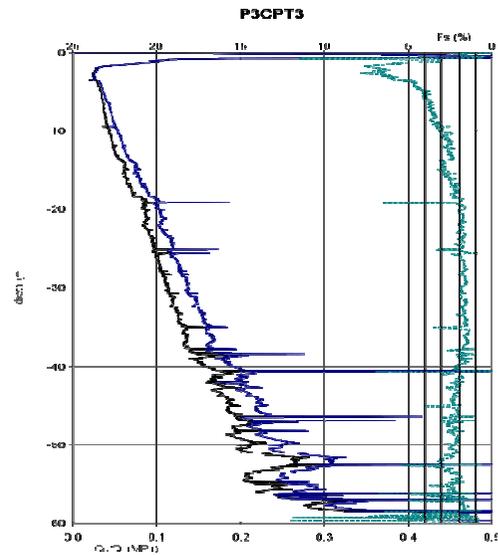
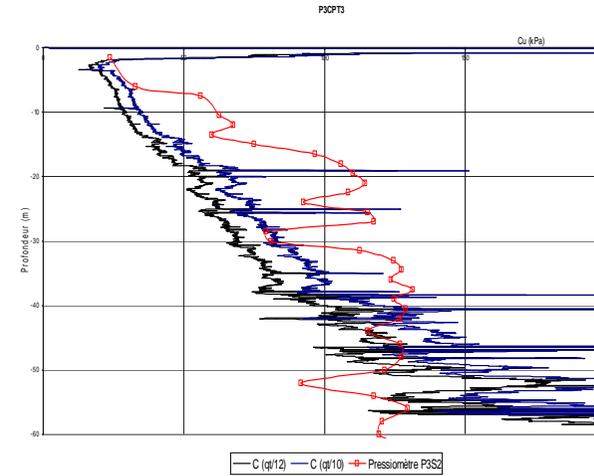
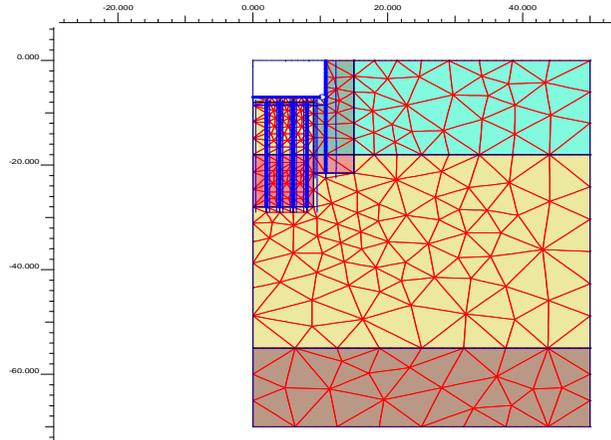
**GTM TP**  
LYON

# P3 & P4 : STIFFENING STRUCTURE WALLS





MONESTIER DE CLERMONT VIADUCT



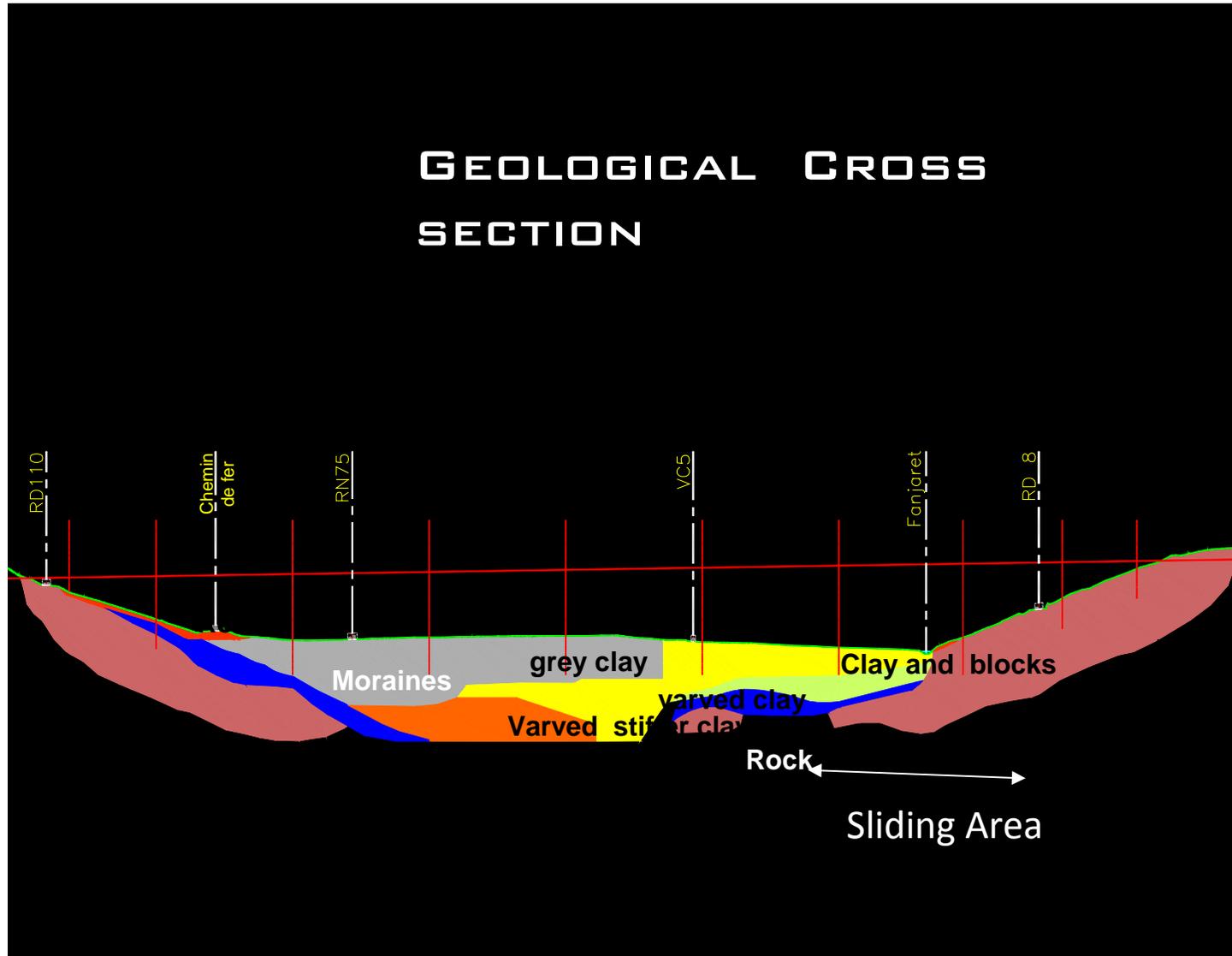
- **P3 to P6**
  - Core borings,
  - CPTU 65 m deep
  - Pressiometric tests
  - Cross hole
  - Pumping test
  - Inclinometres
  - Laboratory tests

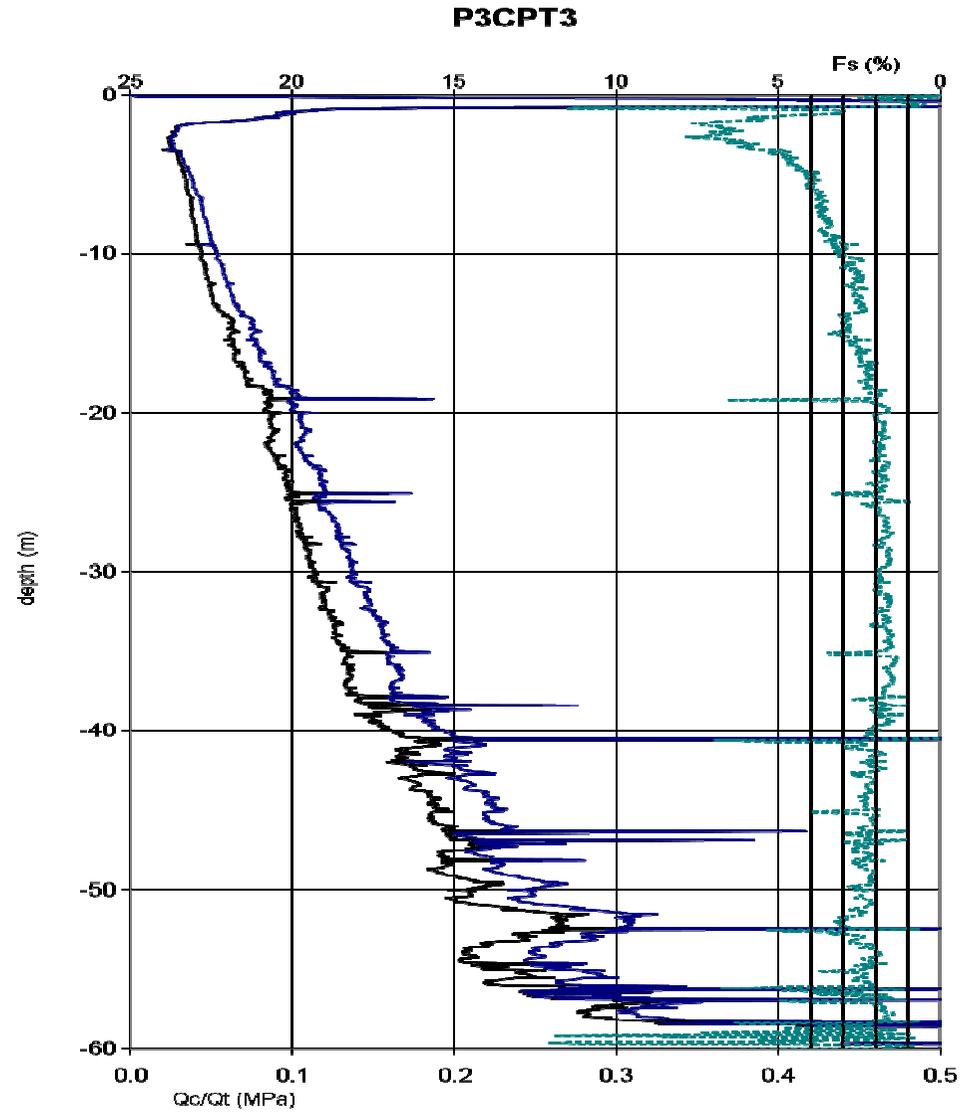


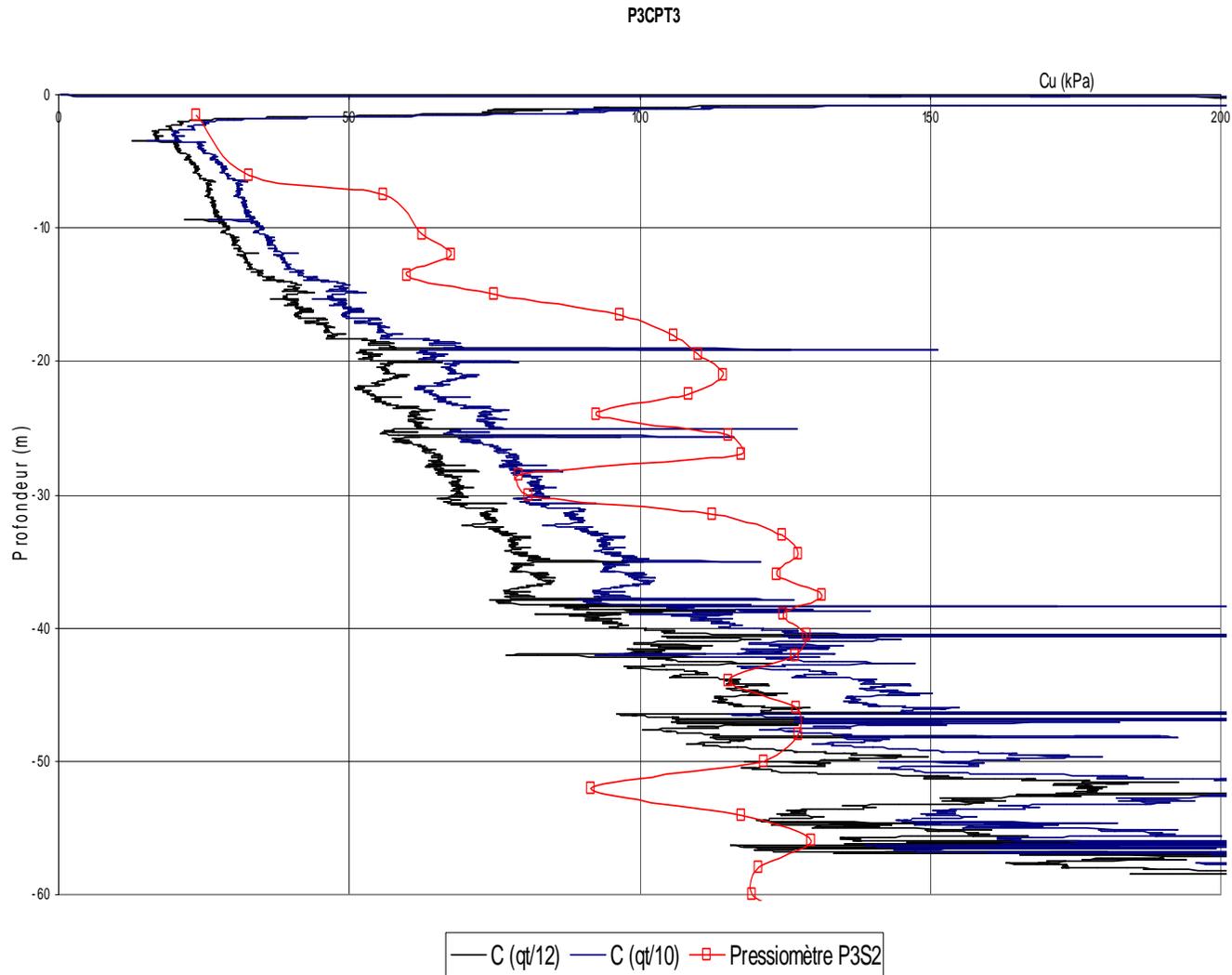
- **Accross the valley:**
  
- **South west area:**
  - Rock at 50 m.
  - Fluvio-glacial permeable till between 40 à 50 m
  - Gravelly clays below soft and remolded clays
  
- **Centre and north of the valley:**
  - Deepening of rock (P2)
  - Argiles homogeneous clays at the surface, varved below



## GEOLOGICAL CROSS SECTION

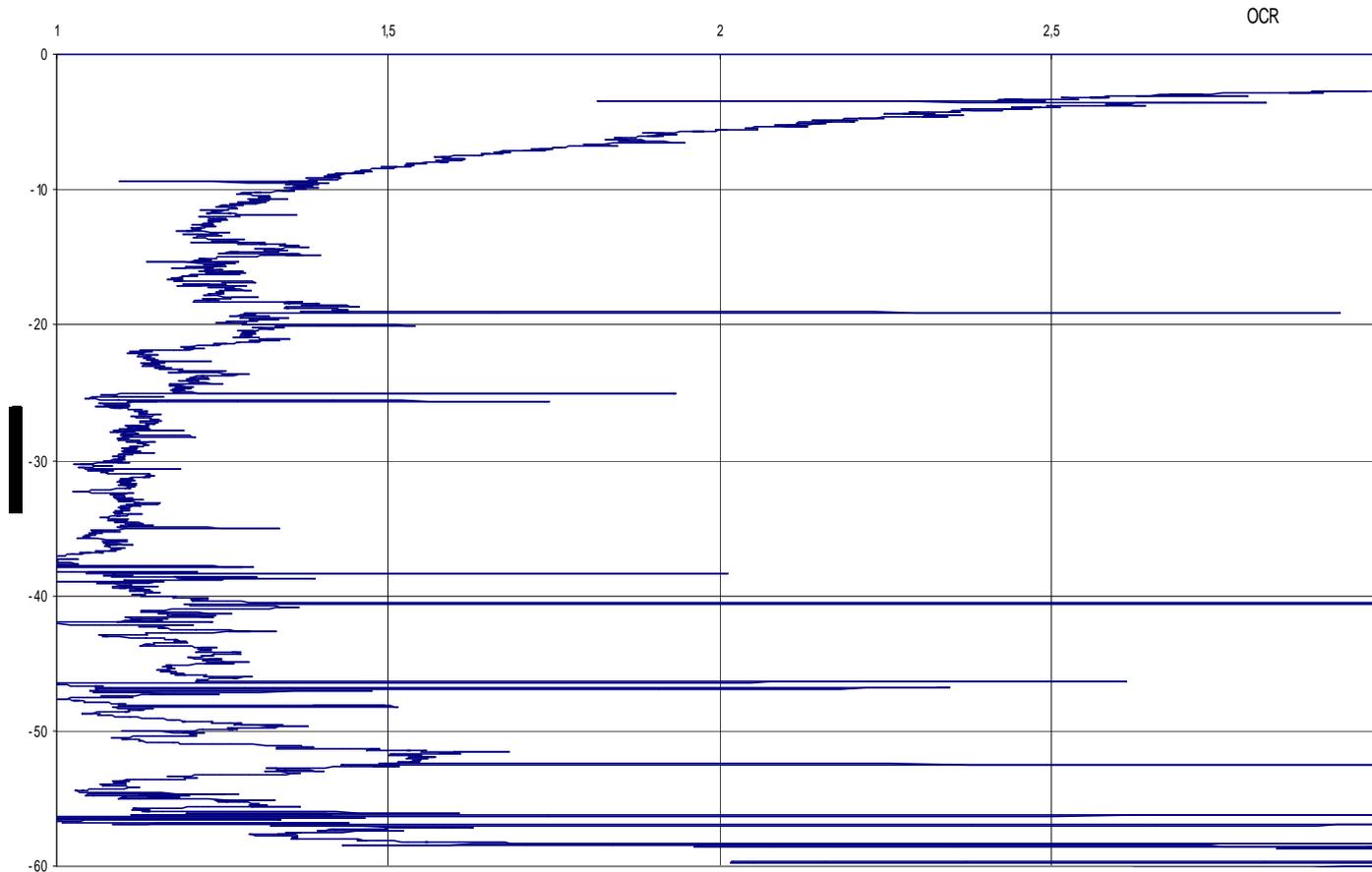


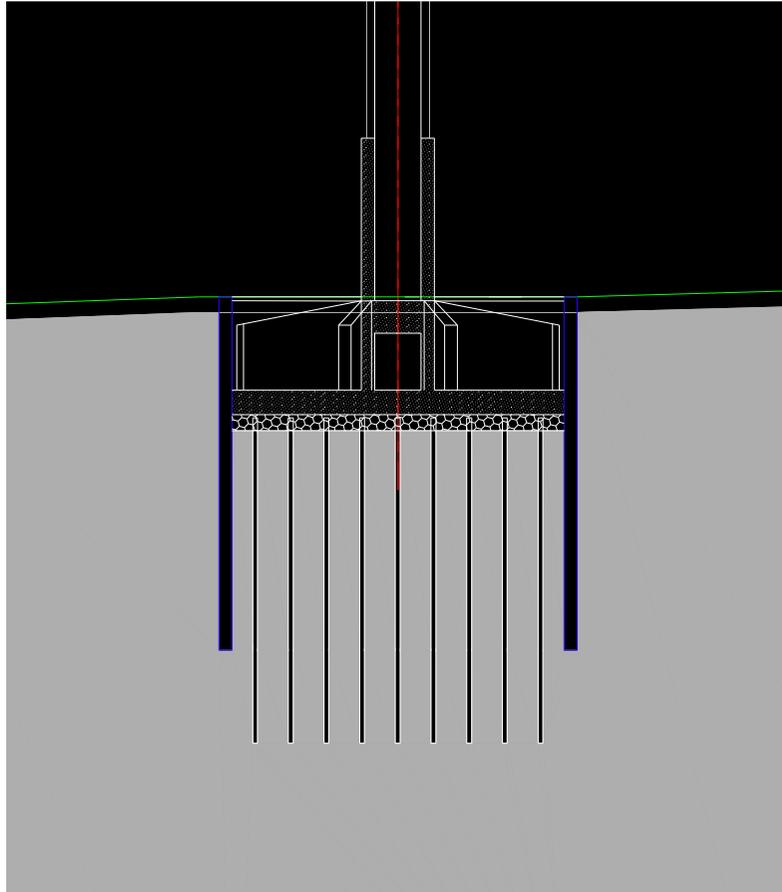






P3CPT3

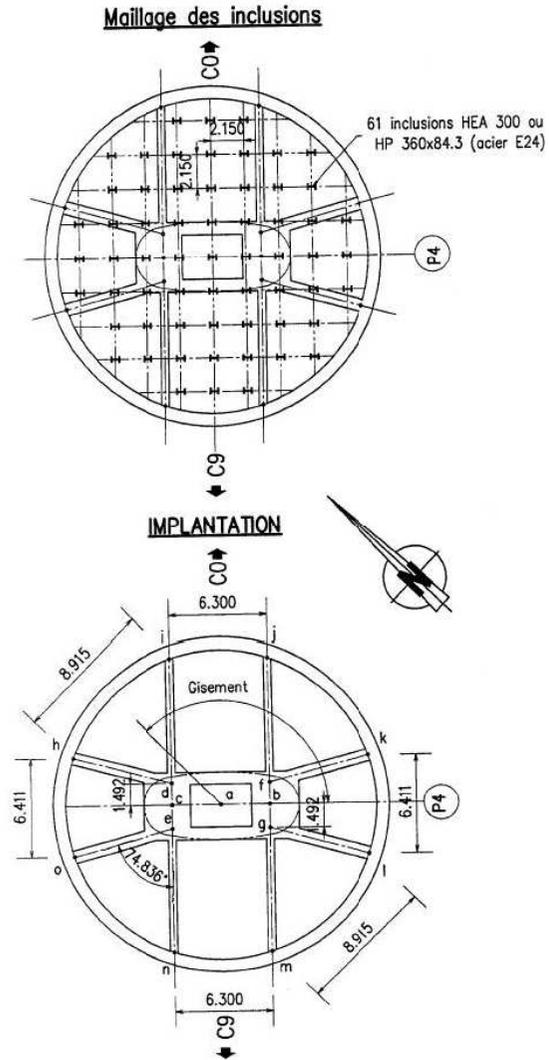




The foundations of P3 and P4 include :

- a cylindrical skirt made of diaphragm wall, 20m diameter and 22 to 26 m deep.
- A 1,50m thick concrete slab
- Steel inclusions (HEA 300), down to 20m below the slab,
- Stiffening walls 80cm thick to transfer the shaft efforts to the slab and the diaphragm walls

An inner volume of 1700m<sup>3</sup> above the slab remains empty.

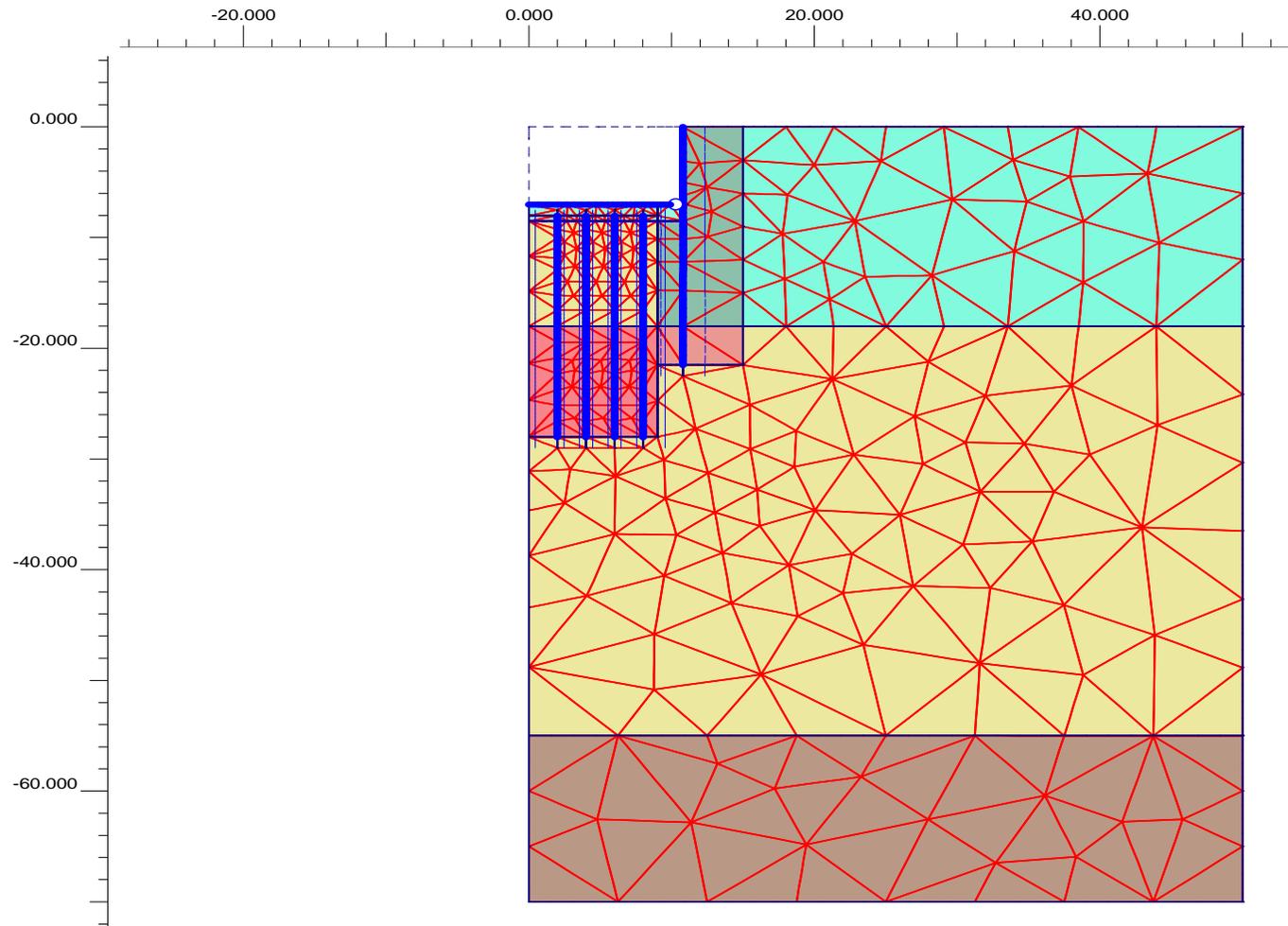


## Strength

Volumetric mass(KN/M <sup>3</sup> )	C' (KN/M <sup>2</sup> )	φ'(°)	OCR	Depth (m)	Type of soil
18.5	5	24	$\sigma'_0 + 50$ KN/M <sup>2</sup>	0 - 18	Upper clay
18.5	0	24	$\sigma'_0$	18 – 37/55	Medium clay
18.5	10	30	1.2 $\sigma'_0$	37/55 - 80	Lower clay

## Deformation

CASE A		CASE B		CASE C		
Triaxial Interpretation		Oedometric Interpretation		Oedometric method		Soil
$E_{50}^{réf}$ (kN/m <sup>2</sup> )	$E_{oed}^{réf}$ (kN/m <sup>2</sup> )	$E_{50}^{réf}$ (kN/m <sup>2</sup> )	$E_{oed}^{réf}$ (kN/m <sup>2</sup> )	$C_c/1+e$	$C_g/1+e$	
7500	6000	3150	2500	0.12	0.024	Upper clay
7500	6000	3150	2500	0.12	0.024	Medium clay
7500	6000	7500	6000	Hardening Model		Lower Clay



- Excavation of a mass of soil close to the estimated load brought by the pier
- Inclusions to control the soil relaxation , reduce the recompression settlement
- Maximum loads during construction ( pre-loading with water)
- After final bearings installation, settlements calculations under final loads and surcharges, consolidation.
- Acceptable differential settlements between piers: 6 cm.

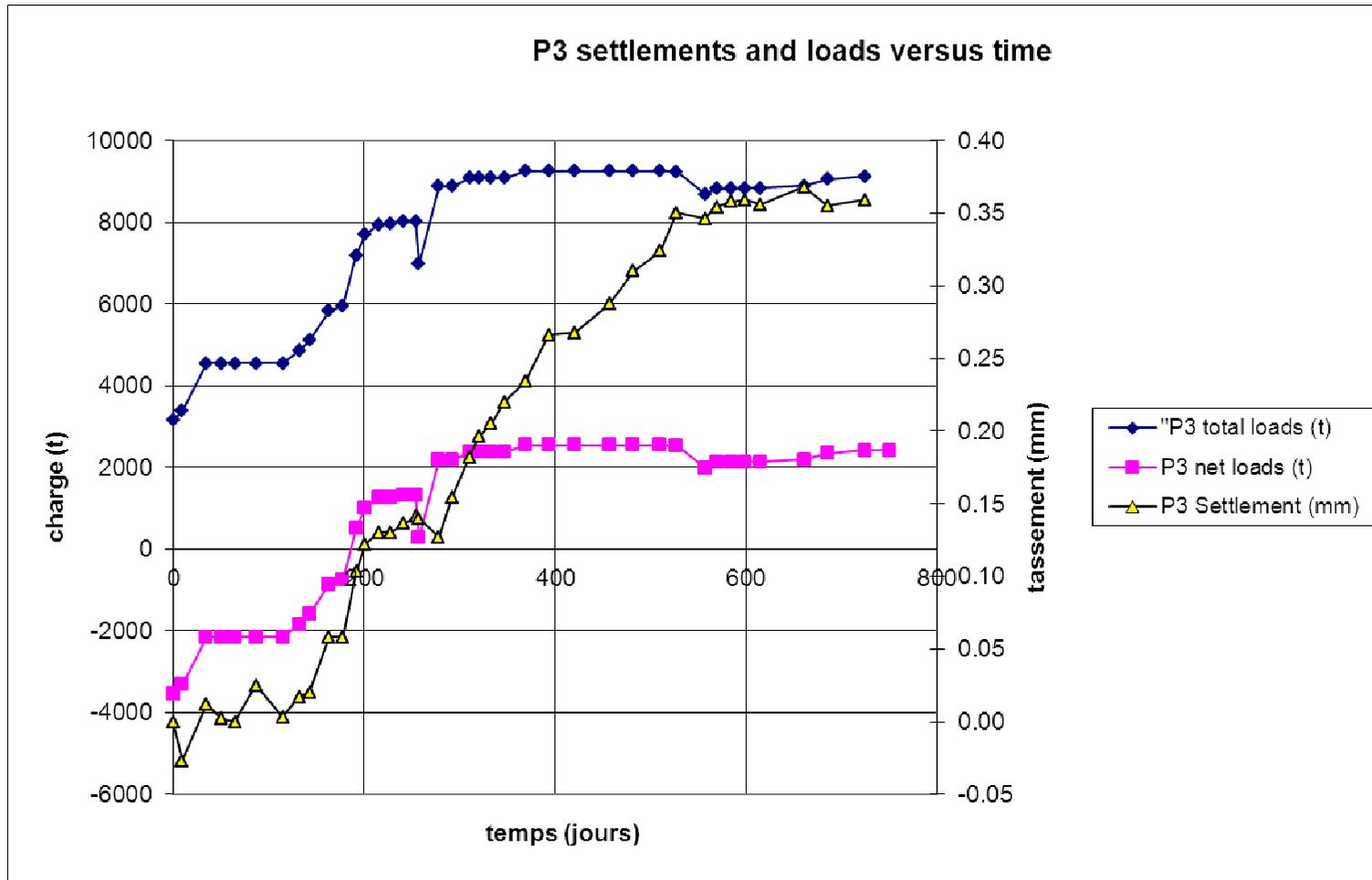
## Design loads

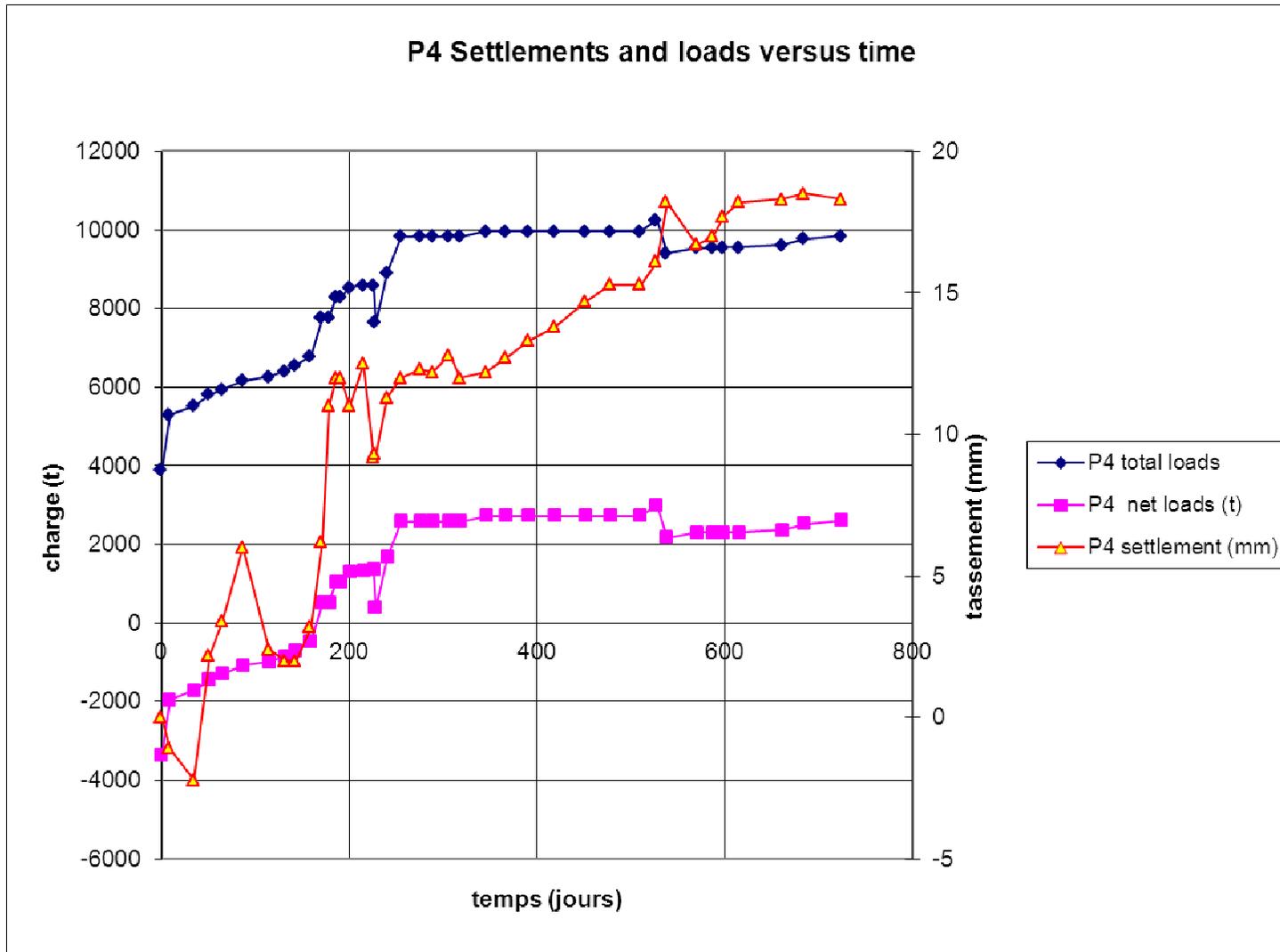
Settlements in mm

Calculation Cases	Soil parametres	Raft construction		Loads without Superstructures + water		Total + service loads + Consolidation	
		P3	P4	P3	P4	P3	P4
A	Triaxial interpretation	5	6	33	35	21	21
B	Triaxial interpretation*0.42	7	6	62	56	50	38
C	Oedometric model	7	7	50	44	30	35

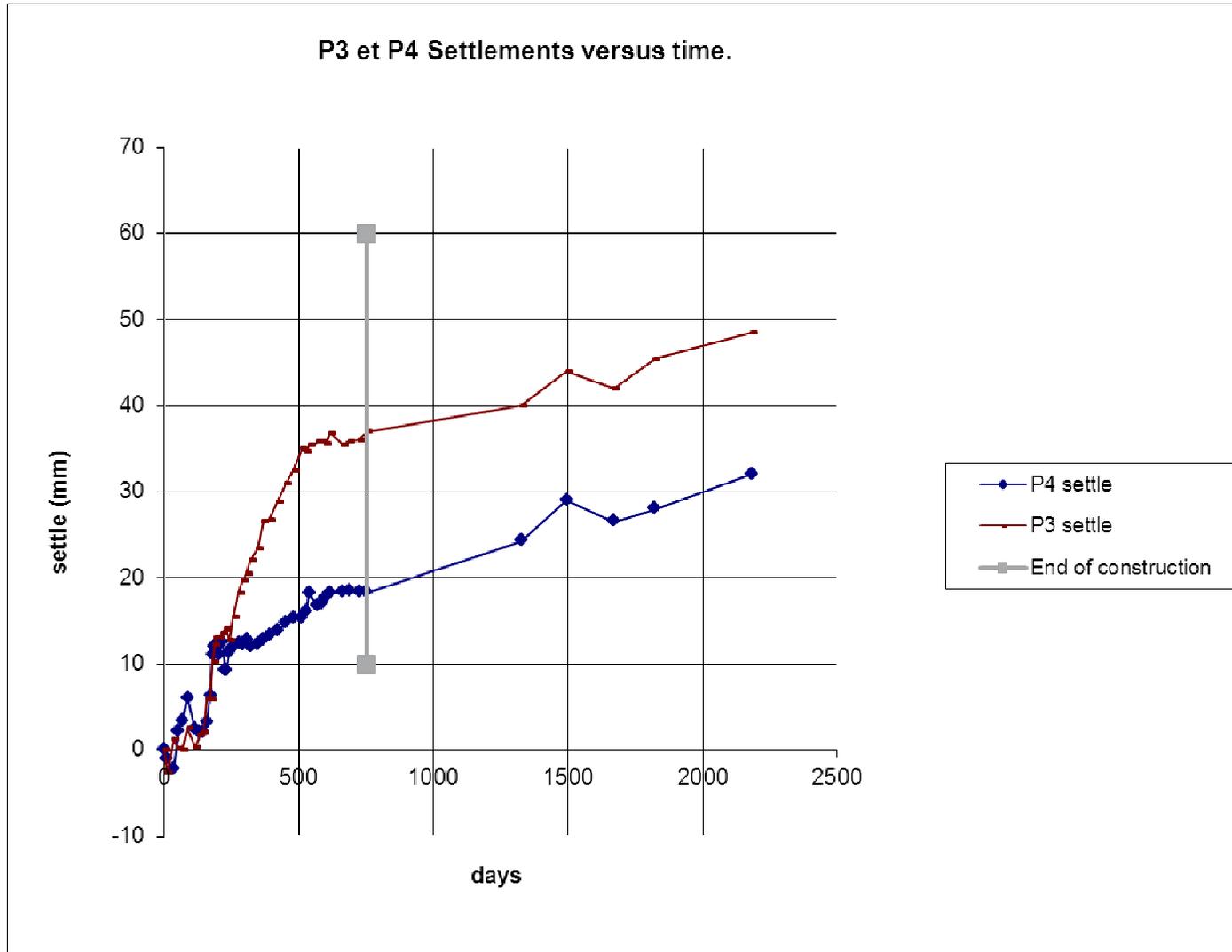
## Deformation

CASE A		CASE B		CASE C		
Triaxial Interpretation		Oedometric Interpretation		Oedometric method		Soil
$E_{50}^{réf}$ (kN/m <sup>2</sup> )	$E_{oed}^{réf}$ (kN/m <sup>2</sup> )	$E_{50}^{réf}$ (kN/m <sup>2</sup> )	$E_{oed}^{réf}$ (kN/m <sup>2</sup> )	$C_c/1+e$	$C_g/1+e$	
7500	6000	3150	2500	0.12	0.024	Upper clay
7500	6000	3150	2500	0.12	0.024	Medium clay
7500	6000	7500	6000	Hardening Model		Lower Clay





- For P3, settlements during construction were close or slightly higher than those estimated with the triaxial interpretation (case A)
- Needs for settlements reductions have been estimated necessary
- Adaptations of the design have been done:
  - Preload with water, removed when superstructures have been completed.
  - Deck level set out 20 mm above designed level to increase the acceptable differential settlements to 80 mm instead of 60 mm initially considered in the design.
- For P4, the settlements are much lower due to the longer length of the diaphragm wall skirt.



## Comparison between estimations and observations

### Settlements in mm

	End of construction		In service	
	P3	P4	P3	P4
<b>Estimations</b>	33 to 62	37 to 56	21*	21*
<b>Observations</b>	37	19	11.5**	13.5**

- \* End of consolidation~ 80 years
- \*\* After ~4 years: Consolidation not completed
- \*\*To be compared to 80 mm acceptable differential settlements

