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Charles-Augustin COULOMB - A geotechnical tribute



spie batignolles

/ fondations



Jean Salençon

Geos

ے SoilCloud





Jean LEHUEROU KERISEL (1908-2005)

ДВУХСОТЛЕТИЕ МЕМУАРА 1773 г. ШАРЛЯ ОГЮСТЕНА КУЛОНА

👘 Проф. Ж. Керизель. Париж, Франция

BICENTENAIRE DE L,ESSAI DE 1773 CHARLES AUGUSTIN COULOMB

J.Kerisel - Professeur Honoraire. Paris, France

BICENTENARY OF THE 1773 PAPER OF CHARLES AUGUSTIN COULOMB

J.Kerisel, Prof. Emeritus, Paris, France.

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Jean Salençon

Académie des sciences Académie des technologies, Paris Senior Fellow HKIAS, City University, Hong Kong

> 250th anniversary of its presentation to the French Academy of Sciences. A most popular landmark text in civil and construction engineering.

Charles-Augustin Coulomb (1736 – 1806)



Member of the French *Académie des sciences* « Section de mécanique » (1795)

"This Memoir, written some years ago, was only intended for my own personal use in the many works I am in charge of. If I now dare to present it to the Academy, it is because it always kindly welcomes the weakest attempt, when it has utility as its object."

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Fort Bourbon As of 1776

ESSAI

Sur une application des règles de Maximis & Minimis à quelques Problèmes de Statique, relatifs à l'Architecture.

Par M. COULOMB, Ingénieur du Roi.

N O T E

On an application of the Rules of Maxima & Minima to some Statics Problems, relevant to

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Coulomb's Memoir Scientific Temporality



Coulomb's Memoir Scientific Temporality



Galileo Galilei (1564 – 1642)





Discorsi

Elasticity: Hooke's Law





Charles-Augustin Coulomb (1736 -1806)



Coulomb's Memoir Scientific Temporality

Stability Analysis



Charles-Augustin Coulomb (1736 -1806)





1788



J-L Lagrange (1736 – 1813)

Stress vector



Resisting forces

(1823) RECHERCHES SUR L'ÉQUILIBRE ET LE MOUVEMENT INTÉRIEUR DES CORPS SOLIDES OU FLUIDES, ÉLASTIQUES OU NON ÉLASTIQUES.

Bulletin de la Sariété Philumntique, p. 9-13; 1823.

Stress tensor



Augustin Louis Cauchy (1789 -1

Fluidity of solids





(1864 - 1870)

Henri-Édouard Tresca (1814 – 1885)



Coulomb's concept of Resistance

"Friction and cohesion are not active forces such as gravity that always fully exerts its effect, but only coercive forces; those two forces are assessed through their limits of resistance".

Du Frottement.

Le frottement & la cohésion ne sont point des forces actives comme la gravité, qui exerce toujours son effet en entier, mais seulement des forces coërcitives; l'on estime ces deux forces par les limites de leur résistance. Lorsqu'on

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Friction

Coulomb refers to Amontons

(1663-1705)

Member of the Académie des sciences (1699)



122 MEMOIRES DE L'ACADEMIE ROYALE

Par ses experiences on peut remarquer, en passant, que c'est une erreur de croire, que les frotemens dans les machines augmentent ou diminuent à proportion que les parties qui frottent, ont plus ou moins d'étenduë, & que la rouë, par exemple, d'un moulin tourne d'autant plus facilement, que ses tourrillons ont moins de longueur, ce qui d'ailleurs est une mauvaise construction, à cause qu'ils mangent incontinent les boëtes dans quoi ils tournent. Mais que ces frottemens augmentent ou diminuent à proportion des fardeaux qui sont mûs, & de la raison de la longeur des leviers qui fervent à les mouvoir à la longueur de ceux fur lesquels ils s'appuïent.

Amontons G., 1699

Moyen de substituer commodément l'action du feu, à la force des hommes et des chevaux pour mouvoir les Machines. *Mémoires de l'Académie Royale des sciences, année* 1699, pp. 112-126.

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"The resistance due to friction is proportional to the pressure exerted"

P cof. *x*; & comme le frottement est proportionnel à la pression, il fera égal à $\frac{P_{\text{cof.}x}}{n}$, *n* étant une quantité constante; friction is proportional to the pressure exerted $1/n = \tan \phi$

Coulomb's own researches on friction would be presented 8 years later



Coulomb C.-A, 1781. Théorie des machines simples en égard au frottement de leurs parties, et à la roideur de leurs cordages. *Recueil des savants étrangers de l'Académie royale des sciences*, 10, 161-332.

Cohesion

Coulomb refers to

van Musschenbroek (1692-1761)

Corresponding Member of the *Académie des sciences* (1734)



De Cobærentia. CAP. XX. De Cohærentia. obærentia vocatur ea corporum con-0. 722. & à quacunque caufa conjunctæ, divulsioni refistunt, ita ut eâdem vi à se mutuo separari nequeant, quâ aut folæ moveri, aut fibi tantummodo impositæ, sejungi iterum potuissent, sed vim postulent multo majorem.

van Musschenbroek P., 1748

Institutiones Physicae conscriptae in usus academicos. Lugduni Batavorum apud Samuelem Luchtmans et filium, Leyden, 1748.

Cohesion

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"Cohesion is measured by the resistance that solid bodies oppose to the direct disunity of their parts. Total cohesion is proportional ... to the fracture surface."

It recalls Galileo's statement

"this consideration dealt with the resistance which all solids offer to fracture and depended upon a certain cement which held the parts glued together so that they would yield and separate only under considerable pull [potente attrazzione]."

Galileo Galilei, 1638. *Dialogues Concerning Two New Sciences*. 20 Crew, H. & Salvio, A. transl., Dover, New York, 1954.

Cohesion + Friction

Two independent additive contributions to material resistance van Musschenbroek

Amontons















ACTIVE and PASSIVE THRUSTS



without causing the triangle to move.



ACTIVE THRUST

a thought experiment



Compatibility Equilibrium Resistance

Force A prevents solid Cba from "flowing" downwards Resisting force fully mobilized upwards along Ba

$$A(\alpha) = \frac{1}{\tan \alpha + \tan \phi} \left(\gamma \frac{a^2}{2 \tan \alpha} (1 - \tan \alpha \tan \phi) - \delta \frac{a}{\cos^2 \alpha} \right)$$

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a thought experiment



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PASSIVE THRUST



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ACTIVE and PASSIVE THRUSTS

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"It has just been proven that, when cohesion and friction both contribute to maintaining the triangle at rest, the limits to the value of a force that can be exerted at point F, perpendicular to CB, without causing the triangle to move, will lie between $A(\alpha)$ and $A'(\alpha)$."



ACTIVE and PASSIVE THRUSTS

Compatibility Equilibrium Resistance

N O T E On an application of the *Rules of* Maxima & Minima to some *Statics Problems, relevant to Architecture.*

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ACTIVE and PASSIVE THRUSTS

"The limits of the horizontal force that can be exerted in F without setting the fluid in motion, will lie between the limits A and A', where A will be a maximum and A'a minimum,"

First appearance of the concept of estimates as a solution to a problem

ACTIVE THRUST

$$A(\alpha) = \frac{1}{\tan \alpha + \tan \phi} \left(\gamma \frac{a^2}{2 \tan \alpha} (1 - \tan \alpha \tan \phi) - \delta \frac{a}{\cos^2 \alpha} \right)$$

Maximized with respect to α

$$\alpha = \pi/4 - \phi/2$$

Coulomb

A lower bound estimate of the maximum pressure exerted on the wall

Non Triangular Wedges

"Up to now, we have assumed that the surface that produces the maximum pressure was triangular; the simplicity of the results derived from this assumption, their easy practical applicability and the desire to be useful and accessible to the Artists, are the reasons that decided for that choice; but if we would want to determine the curve that produces the maximum pressure in an exact way, here is, I think, the way it could be done."

Non Triangular Wedges

Compatibility Equilibrium Resistance

A "slice-method"



Non Triangular Wedges

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PASSIVE THRUST

$$A'(\alpha) = \frac{1}{\tan \alpha + \tan \phi} \left(\gamma \frac{a^2}{2 \tan \alpha} (1 + \tan \alpha \tan \phi) + \delta \frac{a}{\cos^2 \alpha} \right)$$

Minimized with respect to α

$$\alpha = \pi/4 + \phi/2$$

An upper bound estimate of

the resistance opposed by the soil mass to upward impulse



Beyond Coulomb's Analysis



1° Make a clear distinction between the imposed loads exerted on the structure under concern, and the resistances of the constituent materials that can be mobilized under the restrictions imposed by the limits of resistance.

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No energy concept involved

Following Coulomb's track

e.g.,

Fellenius slip-circle method (no complementary assumption for $\phi = 0$) Rendulic log-spiral method (no complementary assumption) Taylor's ϕ -circle method Slice methods

• • •

often call for complementary assumptions about resisting forces ..., to make the problem statically determinate

A kinematical or energy balance viewpoint

Governing idea

Checking a global equilibrium equation, is equivalent to writing that

the work by the "driving" forces exerted on the structure

can be balanced by

the work by resisting forces in the dual rigid body motion, under the constraints imposed by the material limit of resistance.

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A Theory of Yield Design



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Domain of POTENTIAL STABILITY

55

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Principle of virtual work

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A Theory of Yield Design

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Checking a global equilibrium equation, is equivalent to writing that

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Given a potential collapse mechanism

Virtual work by external forces

MAXIMUM resisting work

EQUILIBRIUM AND RESISTANCE ARE MATHEMATICALLY COMPATIBLE



EQUILIBRIUM AND RESISTANCE ARE MATHEMATICALLY COMPATIBLE



EQUILIBRIUM AND RESISTANCE ARE MATHEMATICALLY COMPATIBLE



Either finite or infinite, depending on the potential collapse mechanism A Theory of Yield Design



Either finite or infinite, depending on the potential collapse mechanism

A Theory of Yield Design



Statical Interior approach



MATHEMATICALLY INCOMPATIBLE

Instability is certain

Kinematical Exterior approach







1864-72 Mathematical Theory of Plasticity



1864-72 Mathematical Theory of Plasticity







1948-50



Mathematical Theory of Plasticity






Theory of Yield Design





Mathematical Theory of Plasticity

Plastic Yield Criterion Plastic potential Von Mises Normality Rule Constitutive Equation Plastic Flow Rule

Theory of Yield Design



Mathematical Theory of Plasticity

Plastic Yield Criterion Principle of Maximum Plastic Work Hill **Normality Rule Constitutive Equation Plastic Flow Rule**

Theory of Yield Design



Yield Design or **Plastic Limit Analysis ?**

Mathematical Theory of Plasticity



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Yield Design
or
Plastic Limit Analysis ?
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Mathematical Theory of Plasticity



Theory of Yield Design

Statical interior approach

Potential stability

Extreme loads

Kinematical exterior approach

Mathematical Theory of Plasticity "Lower bound" theorem **Existence** theorem Limit loads "Upper bound" theorem

No Constitutive Law

Normality as a Plastic Constitutive Law

Theory Plastic of Yield Design Limit Analysis "Lower bound" theorem Statical interior approach **Existence** theorem **Potential stability Extreme** loads Limit loads "Upper bound" theorem **Kinematical exterior approach**

No Constitutive Law

Normality as a Plastic Constitutive Law

Within its domain of relevance the theory of Yield Design does not call for the validity of the Normality Rule as a Constitutive Law



As a Conclusion



Governing principles

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Whatever its sophistication which may lead to remarkable theoretical results and whatever the discipline concerned, any mathematical model is only valid insofar as its underlying hypotheses are verified.



THANK YOU for Your Kind Attention

